

# Density, Viscosity, and Electrical Conductivity Measurements on the Ternary System $\text{H}_2\text{O} + \text{C}_2\text{H}_5\text{OH} + \text{LiCl}$ over the Entire Ranges of Solvent Composition and LiCl Solubility from $(-5 \text{ to } +50)^\circ\text{C}$

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Systematic measurements of density, viscosity, and electrical conductivity on the ternary system water + ethanol + lithium chloride over entire ranges of solvent composition and LiCl solubility from  $(-5 \text{ to } +50)^\circ\text{C}$  have been carried out. The temperature-independent aquamolality scale,  $m$  (LiCl moles per 55.5 moles of solvent) has been used to justify data comparison not only at different temperatures but also for the solutions in various solvent mixtures. Density isotherms (fitted to second-order polynomials in  $m$ ) provided a composition-dependent density index,  $g(x_1)$ , which can conveniently be used to determine the density at any desired LiCl concentration, mixture composition, and temperature. Excess molar volumes ( $V^E$ ) of the solvent mixtures have been calculated over the whole temperature range, and minima of all the  $V^E$  isotherms at the same water mole fraction,  $x_1 = 0.6$ , suggest that no significant structural rearrangement takes place in the solvent mixtures upon temperature variation. From the density data, the “temperature average coefficient of thermal expansion” ( $\beta$ ) is also determined for all the samples. Fitting the viscosity ( $\eta$ ) isotherms to an extended Jones-Dole-type cubic equation in  $m$  provided coefficients related to various interactions taking place in the solutions. The temperature dependence of the entire  $\eta$  data can well be explained by the Arrhenius-type equation involving single flow activation energies ( $E_a$ ) that always increased with LiCl concentration for a given solvent but exhibited a sharper rise for the ethanol-rich mixtures;  $E_a$  values tend to pass through maxima at  $x_1 \approx 0.6$ . In all the cases, electrical conductivity ( $\kappa$ ) plotted against  $m$  exhibits maxima which shift from  $4.5m$  to  $\sim 6m$  in the water-rich mixtures, and exhibition of the  $\kappa$ -maxima has been explained with a simple model according to which  $\kappa$  at any given  $m$  is comprised of two sets of the oppositely acting terms, namely  $\kappa_{\text{up}}$  and  $\kappa_{\text{down}}$ . Since all the  $\kappa$  plots fit very well to third-order polynomials in  $m$  with negligibly small coefficients of the cubic terms, the other two terms involving  $m$  and  $m^2$  can be compared with  $\kappa_{\text{up}}$  and  $\kappa_{\text{down}}$ , respectively. From temperature variation of molar conductivity, activation energies have been determined and compared with those of viscous flow.

## Introduction

Propanols and other lower alcohols are completely miscible with water in all proportions at ambient temperatures which allows preparation of their aqueous mixtures of continuously varying properties.<sup>1–4</sup> Structural properties of aqueous alcohols have remained the subject of many investigations.<sup>5–8</sup> Aqueous alcohols are also considered as interesting “solvent systems” for exhibiting relatively higher solubilities of different solutes including electrolytes.<sup>9,10</sup> By maintaining calculated amounts of alcohols as cosolvents in their aqueous mixtures, controlled precipitation of salts can be achieved.<sup>11–14</sup> The significance of the electrolyte solutions in aqueous alcohols has been reported in various investigations of biological interest as well.<sup>15–17</sup> Therefore, data collected on some of the basic properties like density, molar volume, viscosity, electrical conductivity, etc. for aqueous alcohol systems over wide ranges of solvent composition, electrolyte concentration, and temperature can be of great utility. Since water molecules act as a strong ligand<sup>18,19</sup> and tend to selectively solvate ions in the mixtures,<sup>20–22</sup> change of either mixture composition or electrolyte concentration or even temperature may have an influence on the above-mentioned basic properties of the ternary systems.

Besides densities of liquids, also their viscosities over a wide range around ambient temperature have immense importance in solving engineering problems related to heat or mass transfer and fluid dynamics.<sup>23–25</sup> Further, the viscosity variation with temperature and solvent composition are commonly employed as indices for obtaining useful information on structure and interactions within the liquid systems.<sup>24,26,27</sup> Temperature-dependent viscosity studies enable determination of flow activation energy, still another important parameter in chemical research.<sup>28,29</sup> Electrical conductance has always remained important in the investigation of electrolyte solutions, also for its significance toward understanding of the ion–ion, ion–solvent, and even solvent–solvent interactions.<sup>30–32</sup> Conductivity ( $\kappa$ ) is known to depend on factors like temperature, solvent employed, nature of the electrolyte, and its concentration.<sup>33,34</sup> However, the molar conductivity ( $\Lambda_m$ ) being a concentration normalized quantity should not depend on the electrolyte’s concentration unless mutual interactions between the ions start operating.<sup>35</sup>

$\text{H}_2\text{O} + \text{C}_2\text{H}_5\text{OH}$  (*the mixture*) has shown appreciably high solubility for LiCl, while  $\text{H}_2\text{O} + \text{C}_2\text{H}_5\text{OH} + \text{LiCl}$  (*the system*) could sustain up to quite low temperatures without salting out; in addition, *the system* also exhibited some interesting structural and dynamic features.<sup>36</sup> *The system* may have its potential applications in areas like chemical engineering, the automobile industry, biotechnology, medicine, batteries, fuel cells, etc. In

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**Table 1. Densities ( $\rho/\text{g}\cdot\text{cm}^{-3}$ ) at Different Temperatures and LiCl Concentrations in Binary Mixtures of Water (1) and Ethanol (2) Having Mole Fractions  $x_1$  and  $x_2$** 

concentration		temperature, $t/^\circ\text{C}$											
aquamolality/ $m$	molality/ $m$	-5	0	5	10	15	20	25	30	35	40	45	50
$x_1 = 1.0, x_2 = 0.0$													
$\text{g}/10^3 \cdot \text{g}^2 \cdot \text{cm}^{-3} \cdot \text{mol}^{-1} = 0.0223 \pm 0.0006$													
0.0	0.0	—	—	0.9999	0.9997	0.9991	0.9982	0.9971	0.9956	0.9941	0.9922	0.9902	0.9881
0.5	0.5	1.0134	1.0132	1.0137	1.0125	1.0116	1.0108	1.0094	1.0081	1.0066	1.0051	1.0035	1.0022
1.0	1.0	1.0244	1.0244	1.0240	1.0233	1.0222	1.0214	1.0202	1.0187	1.0172	1.0158	1.0138	1.0125
2.0	2.0	1.0471	1.0469	1.0463	1.0453	1.0441	1.0430	1.0418	1.0401	1.0387	1.0371	1.0352	1.0338
3.0	3.0	1.0678	1.0674	1.0664	1.0654	1.0643	1.0631	1.0618	1.0603	1.0587	1.0569	1.0555	1.0390
4.5	4.5	1.0959	1.0950	1.0941	1.0928	1.0915	1.0905	1.0891	1.0877	1.0859	1.0844	1.0830	1.0811
6.0	6.0	1.1217	1.1212	1.1198	1.1188	1.1174	1.1161	1.1146	1.1131	1.1115	1.1101	1.1084	1.1064
8.0	8.0	1.1554	1.1537	1.1526	1.1514	1.1498	1.1485	1.1470	1.1454	1.1439	1.1423	1.1407	1.1388
11.0	11.0	1.2002	1.1987	1.1971	1.1956	1.1940	1.1925	1.1909	1.1893	1.1878	1.1861	1.1843	1.1826
14.0	14.0	1.2407	1.2391	1.2374	1.2358	1.2341	1.2326	1.2307	1.2289	1.2271	1.2253	1.2235	1.2218
17.8	17.8	1.2884	1.2864	1.2842	1.2822	1.2802	1.2783	1.2764	1.2746	1.2728	1.2707	1.2689	1.2669
$x_1 = 0.9, x_2 = 0.1$													
$\text{g}/10^3 \cdot \text{g}^2 \cdot \text{cm}^{-3} \cdot \text{mol}^{-1} = 0.0201 \pm 0.0006$													
0.0	0.0	0.9773	0.9756	0.9732	0.9708	0.9673	0.9637	0.9603	0.9562	0.9527	0.9490	0.9455	0.9420
0.5	0.433	0.9848	0.9834	0.9819	0.9806	0.9786	0.9767	0.9745	0.9721	0.9698	0.9674	0.9643	0.9616
1.0	0.865	0.9965	0.9954	0.9932	0.9913	0.9894	0.9873	0.9851	0.9827	0.9802	0.9776	0.9749	0.9722
2.0	1.730	1.0163	1.0148	1.0128	1.0109	1.0090	1.0070	1.0047	1.0023	0.9999	0.9974	0.9948	0.9922
3.0	2.596	1.0347	1.0331	1.0312	1.0293	1.0273	1.0253	1.0233	1.0213	1.0194	1.0175	1.0154	1.0136
4.5	3.893	1.0606	1.0587	1.0566	1.0548	1.0530	1.0511	1.0490	1.0470	1.0450	1.0430	1.0409	1.0385
6.0	5.191	1.0842	1.0820	1.0800	1.0781	1.0760	1.0739	1.0718	1.0698	1.0678	1.0659	1.0639	1.0619
8.0	6.922	1.1121	1.1101	1.1079	1.1060	1.1039	1.1017	1.0996	1.0977	1.0955	1.0932	1.0911	1.0890
11.0	9.517	1.1507	1.1487	1.1464	1.1441	1.1420	1.1399	1.1376	1.1352	1.1337	1.1315	1.1295	1.1273
14.0	12.113	1.1865	1.1841	1.1820	1.1800	1.1779	1.1759	1.1736	1.1713	1.1693	1.1671	1.1649	1.1628
18.0	15.574	1.2253	1.2227	1.2204	1.2181	1.2159	1.2139	1.2116	1.2096	1.2074	1.2052	1.2030	1.2009
$x_1 = 0.8, x_2 = 0.2$													
$\text{g}/10^3 \cdot \text{g}^2 \cdot \text{cm}^{-3} \cdot \text{mol}^{-1} = 0.0174 \pm 0.0007$													
0.0	0.0	0.9510	0.9480	0.9450	0.9414	0.9380	0.9346	0.9313	0.9276	0.9238	0.9195	0.9155	0.9112
0.5	0.381	0.9615	0.9584	0.9554	0.9518	0.9485	0.9450	0.9419	0.9382	0.9346	0.9305	0.9267	0.9227
1.0	0.763	0.9702	0.9673	0.9641	0.9605	0.9575	0.9541	0.9508	0.9471	0.9437	0.9396	0.9361	0.9322
2.0	1.525	0.9866	0.9836	0.9807	0.9772	0.9741	0.9708	0.9677	0.9642	0.9612	0.9571	0.9538	0.9500
3.0	2.288	1.0011	0.9977	0.9945	0.9909	0.9875	0.9840	0.9809	0.9773	0.9739	0.9697	0.9663	0.9623
4.5	3.431	1.0228	1.0198	1.0168	1.0130	1.0099	1.0066	1.0036	1.0002	0.9969	0.9928	0.9893	0.9855
6.0	4.575	1.0424	1.0394	1.0366	1.0332	1.0303	1.0275	1.0253	1.0224	1.0199	1.0163	1.0135	1.0103
8.0	6.100	1.0683	1.0650	1.0623	1.0590	1.0563	1.0534	1.0511	1.0478	1.0452	1.0419	1.0399	1.0369
11.0	8.388	1.1041	1.1013	1.0988	1.0958	1.0929	1.0903	1.0877	1.0848	1.0821	1.0786	1.0758	1.0726
14.0	10.675	1.1370	1.1343	1.1321	1.1289	1.1264	1.1239	1.1215	1.1186	1.1158	1.1125	1.1097	1.1066
17.5	13.344	1.1735	1.1699	1.1671	1.1637	1.1613	1.1585	1.1561	1.1532	1.1508	1.1477	1.1451	1.1421
$x_1 = 0.7, x_2 = 0.3$													
$\text{g}/10^3 \cdot \text{g}^2 \cdot \text{cm}^{-3} \cdot \text{mol}^{-1} = 0.0152 \pm 0.0005$													
0.0	0.0	0.9316	0.9271	0.9227	0.9187	0.9145	0.9099	0.9053	0.9010	0.8965	0.8920	0.8874	0.8830
0.5	0.341	0.9397	0.9344	0.9300	0.9250	0.9207	0.9156	0.9096	0.9058	0.9012	0.8961	0.8909	0.8859
1.0	0.682	0.9488	0.9425	0.9387	0.9335	0.9289	0.9241	0.9180	0.9144	0.9104	0.9051	0.9001	0.8954
2.0	1.363	0.9627	0.9574	0.9532	0.9493	0.9443	0.9394	0.9336	0.9300	0.9259	0.9208	0.9156	0.9109
3.0	2.045	0.9726	0.9668	0.9625	0.9576	0.9532	0.9485	0.9423	0.9387	0.9343	0.9296	0.9243	0.9195
4.5	3.067	0.9918	0.9863	0.9822	0.9776	0.9736	0.9690	0.9634	0.9600	0.9561	0.9514	0.9467	0.9425
6.0	4.090	1.0116	1.0065	1.0026	0.9980	0.9942	0.9911	0.9852	0.9818	0.9778	0.9736	0.9694	0.9654
8.0	5.453	1.0355	1.0302	1.0266	1.0223	1.0184	1.0142	1.0088	1.0058	1.0026	0.9984	0.9942	0.9906
11.0	7.498	1.0675	1.0614	1.0559	1.0509	1.0477	1.0439	1.0389	1.0355	1.0323	1.0286	1.0248	1.0218
14.0	9.542	1.0978	1.0923	1.0887	1.0845	1.0812	1.0770	1.0718	1.0690	1.0654	1.0620	1.0578	1.0542
16.5	11.246	1.1215	1.1161	1.1123	1.1081	1.1047	1.1007	1.0956	1.0927	1.0895	1.0853	1.0821	1.0787
$x_1 = 0.6, x_2 = 0.4$													
$\text{g}/10^3 \cdot \text{g}^2 \cdot \text{cm}^{-3} \cdot \text{mol}^{-1} = 0.0145 \pm 0.0004$													
0.0	0.0	0.9081	0.9035	0.8993	0.8946	0.8896	0.8851	0.8806	0.8761	0.8714	0.8668	0.8621	0.8573
0.5	0.308	0.9112	0.9065	0.9020	0.8948	0.8889	0.8843	0.8792	0.8744	0.8729	0.8712	0.8705	0.8695
1.0	0.616	0.9184	0.9137	0.9092	0.9022	0.8965	0.8921	0.8872	0.8825	0.8805	0.8791	0.8782	0.8771
2.0	1.232	0.9303	0.9252	0.9206	0.9131	0.9078	0.9047	0.8995	0.8944	0.8924	0.8953	0.8914	0.8884
3.0	1.849	0.9390	0.9341	0.9297	0.9225	0.9168	0.9127	0.9080	0.9034	0.9020	0.9007	0.8999	0.8995
4.5	2.773	0.9571	0.9529	0.9488	0.9420	0.9366	0.9326	0.9281	0.9238	0.9225	0.9215	0.9206	0.9202
6.0	3.697	0.9766	0.9726	0.9684	0.9626	0.9576	0.9544	0.9498	0.9448	0.9436	0.9426	0.9426	0.9424
8.0	4.930	0.9995	0.9954	0.9914	0.9849	0.9799	0.9762	0.9722	0.9682	0.9671	0.9669	0.9670	0.9672
11.0	6.778	1.0317	1.0273	1.0236	1.0169	1.0120	1.0085	1.0043	1.0009	1.0010	1.0006	1.0012	1.0019
14.0	8.627	1.0567	1.0527	1.0488	1.0424	1.0375	1.0346	1.0307	1.0268	1.0253	1.0249	1.0251	1.0277
16.0	9.859	1.0766	1.0724	1.0688	1.0624	1.0578	1.0544	1.0504	1.0466	1.0462	1.0457	1.0460	1.0466
$x_1 = 0.5, x_2 = 0.5$													
$\text{g}/10^3 \cdot \text{g}^2 \cdot \text{cm}^{-3} \cdot \text{mol}^{-1} = 0.0131 \pm 0.0006$													
0.0	0.0	0.8866	0.8821	0.8777	0.8728	0.8685	0.8638	0.8592	0.8548	0.8501	0.8452	0.8405	0.8358
0.5	0.281	0.8880	0.8830	0.8789	0.8722	0.8657	0.8629	0.8571	0.8543	0.8493	0.8435	0.8386	0.8337
1.0	0.562	0.8946	0.8900	0.8867	0.8804	0.8742	0.8716	0.8663	0.8642	0.8592	0.8539	0.8490	0.8443
2.0	1.125	0.9073	0.9033	0.8974	0.8921	0.8863	0.8835	0.8778	0.8753	0.8706	0.8652	0.8594	0.8549
3.0	1.687	0.9169	0.9136	0.9092	0.9008	0.8973	0.8933	0.8876	0.8845	0.8798	0.8745	0.8668	0.8623

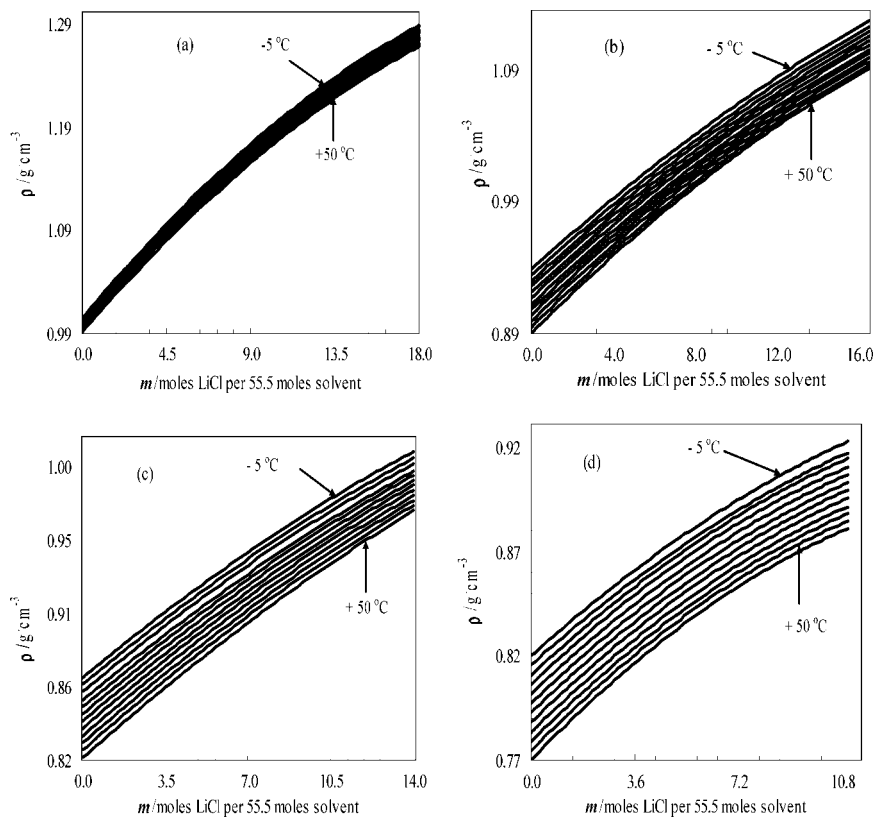
Table 1 Continued

concentration		temperature, $t/^\circ\text{C}$											
aquamolality/ $m$	molality/ $m$	-5	0	5	10	15	20	25	30	35	40	45	50
4.5	2.530	0.9307	0.9261	0.9220	0.9155	0.9091	0.9067	0.9012	0.8988	0.8941	0.8888	0.8839	0.8794
6.0	3.374	0.9489	0.9442	0.9406	0.9347	0.9288	0.9259	0.9206	0.9185	0.9141	0.9091	0.9045	0.9004
8.0	4.498	0.9706	0.9663	0.9628	0.9568	0.9507	0.9488	0.9437	0.9418	0.9376	0.9325	0.9282	0.9241
11.0	6.185	0.9977	0.9931	0.9893	0.9837	0.9778	0.9758	0.9705	0.9688	0.9647	0.9602	0.9562	0.9528
14.0	7.872	1.0248	1.0206	1.0170	1.0113	1.0056	1.0036	0.9988	0.9970	0.9929	0.9882	0.9842	0.9807
15.2	8.547	1.0376	1.0333	1.0297	1.0239	1.0181	1.0162	1.0114	1.0097	1.0062	1.0016	0.9973	0.9943
$x_1 = 0.4, x_2 = 0.6$													
$\text{g}/10^3 \cdot \text{g}^2 \cdot \text{cm}^{-3} \cdot \text{mol}^{-1} = 0.0133 \pm 0.0008$													
0.0	0.0	0.8677	0.8634	0.8588	0.8541	0.8495	0.845	0.8406	0.8361	0.8314	0.8269	0.8224	0.8177
0.5	0.259	0.8667	0.8620	0.8576	0.8510	0.8474	0.8428	0.8385	0.8340	0.8287	0.8242	0.8197	0.8139
1.0	0.517	0.8729	0.8687	0.8641	0.8578	0.8545	0.8497	0.8457	0.8409	0.8356	0.8309	0.8264	0.8213
2.0	1.034	0.8858	0.8811	0.8768	0.8704	0.8672	0.8625	0.8585	0.8541	0.8489	0.8446	0.8406	0.8357
3.0	1.551	0.8977	0.8934	0.8890	0.8829	0.8800	0.8755	0.8708	0.8676	0.8627	0.8589	0.8547	0.8496
4.5	2.327	0.9106	0.9052	0.9013	0.8929	0.8894	0.8858	0.8814	0.8772	0.8735	0.8682	0.8636	0.8580
6.0	3.102	0.9242	0.9202	0.9165	0.9101	0.9073	0.9029	0.8993	0.8952	0.8906	0.8866	0.8826	0.8778
8.0	4.136	0.9462	0.9418	0.9375	0.9313	0.9288	0.9247	0.9211	0.9171	0.9124	0.9084	0.9047	0.9000
11.0	5.687	0.9753	0.9710	0.9672	0.9613	0.9587	0.9547	0.9515	0.9481	0.9435	0.9399	0.9367	0.9321
14.0	7.238	0.9998	0.9955	0.9917	0.9862	0.9842	0.9804	0.9779	0.9745	0.9707	0.9675	0.9643	0.9607
$x_1 = 0.3, x_2 = 0.7$													
$\text{g}/10^3 \cdot \text{g}^2 \cdot \text{cm}^{-3} \cdot \text{mol}^{-1} = 0.0134 \pm 0.0008$													
0.0	0.0	0.8522	0.8477	0.8429	0.8385	0.8339	0.8294	0.8251	0.8206	0.816	0.8111	0.8066	0.8019
0.5	0.239	0.8495	0.8447	0.8403	0.8358	0.8311	0.8272	0.8228	0.8175	0.8128	0.8074	0.8027	0.7978
1.0	0.479	0.8559	0.8509	0.8465	0.8419	0.8368	0.8332	0.8286	0.8233	0.8187	0.8138	0.8091	0.8038
2.0	0.957	0.8673	0.8624	0.8582	0.8539	0.8491	0.8454	0.8409	0.8359	0.8314	0.8263	0.8219	0.8175
3.0	1.436	0.8787	0.8743	0.8700	0.8661	0.8613	0.8575	0.8532	0.8486	0.8444	0.8396	0.8355	0.8317
4.5	2.153	0.8963	0.8912	0.8873	0.8833	0.8787	0.8753	0.8709	0.8662	0.8621	0.8573	0.8527	0.8487
6.0	2.871	0.9116	0.9074	0.9034	0.9000	0.8956	0.8921	0.8881	0.8836	0.8796	0.8750	0.8709	0.8665
8.0	3.828	0.9276	0.9234	0.9197	0.9160	0.9117	0.9080	0.9038	0.8999	0.8967	0.8915	0.8875	0.8836
11.0	5.264	0.9536	0.9492	0.9452	0.9416	0.9374	0.9343	0.9305	0.9263	0.9226	0.9186	0.9152	0.9114
13.5	6.460	0.9757	0.9713	0.9672	0.9634	0.9591	0.9560	0.9526	0.9486	0.9449	0.9408	0.9373	0.9332
$x_1 = 0.2, x_2 = 0.8$													
$\text{g}/10^3 \cdot \text{g}^2 \cdot \text{cm}^{-3} \cdot \text{mol}^{-1} = 0.0132 \pm 0.0007$													
0.0	0.0	0.8382	0.8337	0.829	0.8247	0.8201	0.8156	0.811	0.806	0.8014	0.7968	0.7922	0.7875
0.5	0.223	0.8369	0.8320	0.8277	0.8229	0.8174	0.8128	0.8072	0.8019	0.7973	0.7903	0.7873	0.7842
1.0	0.445	0.8435	0.8381	0.8350	0.8278	0.8227	0.8188	0.8140	0.8084	0.8043	0.7976	0.7949	0.7912
2.0	0.891	0.8544	0.8504	0.8462	0.8404	0.8350	0.8308	0.8260	0.8210	0.8166	0.8100	0.8074	0.8040
3.0	1.336	0.8647	0.8605	0.8568	0.8513	0.8461	0.8422	0.8373	0.8324	0.8282	0.8222	0.8200	0.8177
4.5	2.004	0.8812	0.8770	0.8733	0.8681	0.8628	0.8591	0.8545	0.8499	0.8459	0.8398	0.8375	0.8343
6.0	2.672	0.8965	0.8924	0.8890	0.8840	0.8789	0.8752	0.8707	0.8660	0.8620	0.8558	0.8534	0.8505
8.0	3.563	0.9159	0.9124	0.9095	0.9045	0.8994	0.8959	0.8915	0.8870	0.8832	0.8771	0.8744	0.8719
11.0	4.899	0.9394	0.9335	0.9304	0.9255	0.9218	0.9170	0.9129	0.9086	0.9069	0.8977	0.8952	0.8951
13.0	5.789	0.9534	0.9497	0.9463	0.9414	0.9367	0.9332	0.9287	0.9242	0.9207	0.9147	0.9129	0.9104
$x_1 = 0.1, x_2 = 0.9$													
$\text{g}/10^3 \cdot \text{g}^2 \cdot \text{cm}^{-3} \cdot \text{mol}^{-1} = 0.0133 \pm 0.0006$													
0.0	0.0	0.8249	0.8203	0.8159	0.8114	0.8069	0.8021	0.7977	0.793	0.7882	0.7836	0.779	0.7743
0.5	0.208	0.823	0.8172	0.8129	0.8084	0.8035	0.7988	0.7941	0.7891	0.784	0.7795	0.775	0.7701
1.0	0.416	0.827	0.8226	0.8185	0.8145	0.8095	0.8048	0.8002	0.7954	0.7903	0.786	0.7817	0.7785
2.0	0.833	0.8387	0.8341	0.8304	0.8258	0.8213	0.8165	0.8118	0.807	0.8021	0.7981	0.7937	0.7895
3.0	1.249	0.8506	0.8451	0.8409	0.8373	0.8322	0.8276	0.8232	0.8187	0.8139	0.8101	0.806	0.8022
4.5	1.874	0.8638	0.8576	0.854	0.8494	0.8443	0.8398	0.8349	0.8304	0.826	0.822	0.8195	0.816
6.0	2.499	0.8802	0.8754	0.8722	0.8685	0.8641	0.8595	0.8558	0.8514	0.847	0.8433	0.8394	0.8355
8.0	3.332	0.8983	0.8922	0.8923	0.8883	0.8842	0.8797	0.8757	0.8715	0.8671	0.8635	0.8597	0.8558
11.0	4.581	0.9175	0.9114	0.9079	0.9034	0.8994	0.8952	0.8915	0.8872	0.8828	0.8794	0.8759	0.8724
$x_1 = 0.0, x_2 = 1.0$													
$\text{g}/10^3 \cdot \text{g}^2 \cdot \text{cm}^{-3} \cdot \text{mol}^{-1} = 0.0131 \pm 0.0008$													
0.0	0.0	0.8111	0.8068	0.8026	0.7984	0.7942	0.7899	0.7857	0.7814	0.7771	0.7728	0.7679	0.7634
0.5	0.196	0.8109	0.8051	0.8032	0.7961	0.7897	0.786	0.7824	0.7765	0.7738	0.773	0.7722	0.7687
1.0	0.391	0.8179	0.8106	0.8103	0.8009	0.7959	0.7919	0.7883	0.7825	0.7797	0.779	0.7786	0.7743
2.0	0.782	0.8284	0.8213	0.8215	0.8122	0.8075	0.8033	0.7994	0.7947	0.7912	0.7907	0.7909	0.7861
3.0	1.173	0.8381	0.8325	0.8341	0.8234	0.8175	0.8136	0.8103	0.8048	0.8023	0.8019	0.8018	0.7966
4.5	1.760	0.8545	0.847	0.8455	0.8374	0.8316	0.8288	0.8238	0.8195	0.8166	0.8158	0.8168	0.811
6.0	2.347	0.8694	0.8631	0.8645	0.8542	0.8491	0.8454	0.8423	0.8371	0.8356	0.8352	0.8349	0.8304
8.0	3.129	0.8877	0.8824	0.8836	0.8757	0.8684	0.8647	0.8619	0.8567	0.8547	0.8547	0.8539	0.8513
10.0	3.911	0.9078	0.9011	0.9021	0.8918	0.8869	0.8834	0.8805	0.8754	0.8736	0.8737	0.874	0.8694

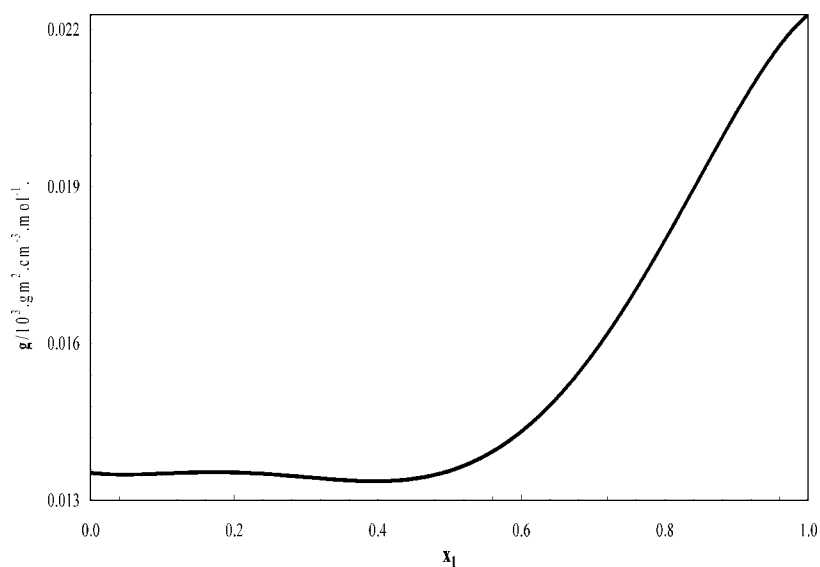
the present work, comprehensive data on density ( $\rho$ ), viscosity ( $\eta$ ), and electrical conductivity ( $\kappa$ ) for the system have been presented over the entire ranges of solvent composition and LiCl solubility from (-5 to +50) °C. Excess molar volumes ( $V^E$ ) for the mixture at a series of compositions have also been determined whose isotherms exhibit minima at the same common water mole fraction ( $x_1$ ) of 0.6. From the temperature dependence of  $\eta$  and  $\Lambda_m$ , respective activation energies have been determined and mutually compared. In the case that conductivity is only governed by the solution viscosity, a correspondence should exist between the activation energies determined for the viscosity and conductivity.

## Experimental Section

**Chemicals and Preparation of Samples.** Chemicals of high grade purity were employed for the study. Water (room-temperature electrical conductivity between (1 and 2)  $\mu\text{S} \cdot \text{cm}^{-1}$ ) used as one of the solvent components was freshly prepared after double distillation carried out in an all-quickfit apparatus in the presence of a few crystals of  $\text{KMnO}_4$  and a small amount of  $\text{NaOH}$ .<sup>37</sup> Ethanol (Merck, purity  $\geq 99\%$ ) was used without further drying because all the LiCl solutions were to be prepared in the mixtures (except those in neat ethanol). A proton NMR spectrum of the ethanol measured at 32 °C exhibited no extra



**Figure 1.** (a–d) Densities,  $\rho$ , fitted to LiCl aquamolality,  $m$ , in the isotherm:  $\rho(m) = d_0 + d_1 \cdot m + d_2 \cdot m^2$  from  $-5$  to  $+50$  at  $5$  °C intervals for solutions prepared in aqueous ethanol of water mole fractions  $x_1 =$ : (a) 1.0, (b) 0.7, (c) 0.4, and (d) 0.1 (refer to Table 2 for  $d$  values).



**Figure 2.** Dependence of the density index,  $g(x_1)$ , on water mole fractions,  $x_1$ , for the system  $\text{H}_2\text{O} + \text{C}_2\text{H}_5\text{OH} + \text{LiCl}$ .

peak, and also a triplet peak was observed for its OH.<sup>38,39</sup> “Anhydrous” LiCl (Merck, purity > 99 % also verified by atomic absorption spectrophotometry) employed in the study was first kept in an electric oven at about  $200$  °C for several hours and finally stored in a desiccator under low pressure.

Suitable volumes of the samples were carefully prepared (with minimum possible atmospheric exposure) by adding together precalculated amounts of the individual components in closed vessels and subsequently stored in sealed bottles. An ER-180A digital balance from A & D, Japan (detection limit  $0.1$  mg) was employed for the weighings. As in many previous works,<sup>36,40–43</sup> the solute (LiCl) concentration has been expressed in the

temperature-independent aquamolality scale,  $m$  (moles of solute per 55.5 moles of the solvent).

**Temperature Controlling.** All the density measurements were carried out in thermostatic conditions. For the set of measurements on a given sample, temperature was successively raised through intervals of  $5$  °C over the employed range from  $(-5$  to  $+50)$  °C. The required temperature of the sample (submerged in a bath of a water–ethanol mixture) was maintained by circulating the mixture using a (HAAKE F3, Germany) chiller equipped with an automatic temperature-controlling sensor having a detection limit of  $\pm 0.02$  °C. Besides a digital display on the chiller, the bath temperature was also simultaneously

**Table 2. Coefficients (in Appropriate Units) of the Equation  $\rho(t, m) = d_0(t) + d_1(t) \cdot m + d_2(t) \cdot m^2$  at Different Temperatures in Binary Mixtures of Water (1) and Ethanol (2) Having Mole Fractions  $x_1$  and  $x_2$  with  $m$  Being the LiCl Aquamolality**

coefficients	temperature, $t/^\circ\text{C}$											
	-5	0	5	10	15	20	25	30	35	40	45	50
$x_1 = 1.0, x_2 = 0.0$												
$d_0$	1.0029	1.0031	1.0000	0.9996	0.9993	0.9981	0.9970	0.9958	0.9942	0.9921	0.9900	0.9882
$d_1$	0.0218	0.0216	0.0221	0.0220	0.0217	0.0217	0.0217	0.0216	0.0216	0.0218	0.0219	0.0214
$d_2$	-0.0003	-0.0003	-0.0004	-0.0004	-0.0003	-0.0003	-0.0003	-0.0003	-0.0003	-0.0004	-0.0004	-0.0003
$x_1 = 0.9, x_2 = 0.1$												
$d_0$	0.9746	0.9733	0.9719	0.9700	0.9682	0.9660	0.9641	0.9614	0.9589	0.9563	0.9532	0.9501
$d_1$	0.0202	0.0201	0.0199	0.0200	0.0199	0.0199	0.0199	0.0200	0.0202	0.0203	0.0205	0.0207
$d_2$	-0.0004	-0.0004	-0.0003	-0.0003	-0.0003	-0.0003	-0.0003	-0.0004	-0.0004	-0.0004	-0.0004	-0.0004
$x_1 = 0.8, x_2 = 0.2$												
$d_0$	0.9519	0.9489	0.9459	0.9423	0.9389	0.9355	0.9322	0.9285	0.9247	0.9204	0.9164	0.9121
$d_1$	0.0164	0.0165	0.0165	0.0165	0.0166	0.0167	0.0168	0.0169	0.0171	0.0173	0.0175	0.0177
$d_2$	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0003	-0.0003
$x_1 = 0.7, x_2 = 0.3$												
$d_0$	0.9325	0.9280	0.9236	0.9196	0.9154	0.9108	0.9062	0.9019	0.8974	0.8929	0.8883	0.8839
$d_1$	0.0143	0.0143	0.0145	0.0145	0.0146	0.0148	0.0149	0.0151	0.0154	0.0156	0.0157	0.0160
$d_2$	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002
$x_1 = 0.6, x_2 = 0.4$												
$d_0$	0.9090	0.9044	0.9002	0.8955	0.8905	0.8860	0.8815	0.8770	0.8723	0.8677	0.8630	0.8582
$d_1$	0.0126	0.0128	0.0128	0.0127	0.0129	0.0132	0.0133	0.0134	0.0140	0.0149	0.0155	0.0163
$d_2$	-0.0001	-0.0001	-0.0001	-0.0001	-0.0001	-0.0001	-0.0001	-0.0001	-0.0002	-0.0002	-0.0002	-0.0003
$x_1 = 0.5, x_2 = 0.5$												
$d_0$	0.8866	0.8821	0.8777	0.8728	0.8685	0.8638	0.8592	0.8548	0.8501	0.8452	0.8405	0.8358
$d_1$	0.0121	0.0123	0.0124	0.0123	0.0123	0.0127	0.0127	0.0131	0.0132	0.0134	0.0133	0.0135
$d_2$	-0.0001	-0.0001	-0.0001	-0.0001	-0.0001	-0.0001	-0.0001	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002
$x_1 = 0.4, x_2 = 0.6$												
$d_0$	0.8677	0.8634	0.8588	0.8541	0.8495	0.8450	0.8406	0.8361	0.8314	0.8269	0.8224	0.8177
$d_1$	0.0124	0.0124	0.0126	0.0123	0.0126	0.0128	0.0128	0.013	0.0132	0.0133	0.0134	0.0134
$d_2$	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002
$x_1 = 0.3, x_2 = 0.7$												
$d_0$	0.8522	0.8477	0.8429	0.8385	0.8339	0.8294	0.8251	0.8206	0.8160	0.8111	0.8066	0.8019
$d_1$	0.0122	0.0123	0.0125	0.0127	0.0129	0.0131	0.0131	0.0132	0.0134	0.0136	0.0137	0.0139
$d_2$	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0002	-0.0003
$x_1 = 0.2, x_2 = 0.8$												
$d_0$	0.8382	0.8337	0.8290	0.8247	0.8201	0.8156	0.8110	0.8060	0.8014	0.7968	0.7922	0.7875
$d_1$	0.0125	0.0126	0.0129	0.0128	0.0128	0.0130	0.0131	0.0134	0.0135	0.0134	0.0138	0.0143
$d_2$	-0.0002	-0.0002	-0.0003	-0.0002	-0.0002	-0.0002	-0.0003	-0.0003	-0.0003	-0.0003	-0.0003	-0.0003
$x_1 = 0.1, x_2 = 0.9$												
$d_0$	0.8249	0.8203	0.8159	0.8114	0.8069	0.8021	0.7977	0.7930	0.7882	0.7836	0.7790	0.7743
$d_1$	0.0120	0.0121	0.0124	0.0127	0.0127	0.0129	0.0129	0.0131	0.0133	0.0135	0.0139	0.0142
$d_2$	-0.0003	-0.0003	-0.0003	-0.0003	-0.0003	-0.0003	-0.0003	-0.0003	-0.0003	-0.0003	-0.0004	-0.0004
$x_1 = 0.0, x_2 = 1.0$												
$d_0$	0.8111	0.8068	0.8026	0.7984	0.7942	0.7899	0.7857	0.7814	0.7771	0.7728	0.7679	0.7634
$d_1$	0.0125	0.0120	0.0127	0.0120	0.0116	0.0119	0.0119	0.0119	0.0122	0.0130	0.0143	0.0141
$d_2$	-0.0002	-0.0002	-0.0002	-0.0002	-0.0001	-0.0002	-0.0001	-0.0001	-0.0002	-0.0002	-0.0003	-0.0003

monitored using an ASTM-calibrated thermometer [(0 to 100)  $^\circ\text{C}$ ] having a graduation of 0.01  $^\circ\text{C}$ . Although samples attained the required temperatures in about 10 min, they were allowed to thermally equilibrate in the bath for at least 20 min before starting the measurements.

**Density Measurement.** Densities were determined using 10 mL Pyrex density bottles which were calibrated at each working temperature by employing water and toluene (Merck, purity > 99.9 %) as references. Toluene was used without further purification as it did not exhibit any extra peak in its NMR spectrum. The sample and the density bottles were allowed to attain equilibrium in the preadjusted thermal bath. Since the laboratory temperature was maintained around 25  $^\circ\text{C}$  throughout the experiments, the colder baths were accordingly adjusted at slightly lower than the required temperatures to allow compensation due to heat exchange during weighing of the density bottle (and conversely at higher temperatures for the hotter baths); nevertheless, weighings were done swiftly, and all readings were repeated at least three times. Whereas the maximum difference

of the required and actual temperatures could be  $\pm 0.1$   $^\circ\text{C}$ , uncertainty in the density value could be  $\pm 0.0002$   $\text{g}\cdot\text{cm}^{-3}$ . Some selected density values at various temperatures were also monitored on a DMA-4500, Anton Paar (Austria) vibrating tube density meter having a resolution<sup>44</sup> of  $5\cdot 10^{-5}$   $\text{g}\cdot\text{cm}^{-3}$ . The density values up to the fourth decimal position were in agreement with our two kinds of measurements.

**Viscosity Measurement.** Viscosities at different temperatures were measured in a specially designed transparent glass bath which ensured placing of the viscometer and an ASTM-calibrated thermometer at their same respective positions during each measurement. The bath temperature was maintained by circulating the thermostatted ethanol–water mixture through it. For each measurement, a 20 mL sample loaded in the viscometer was first allowed to attain the required temperature in the bath. Since viscosity values covered a considerably wide range (from (0.55 to 181) mPa·s) on varying temperature and LiCl concentration in our study, Ubbelohde viscometers (each  $\sim 20$  mL capacity) of three different capillary bores were employed. The

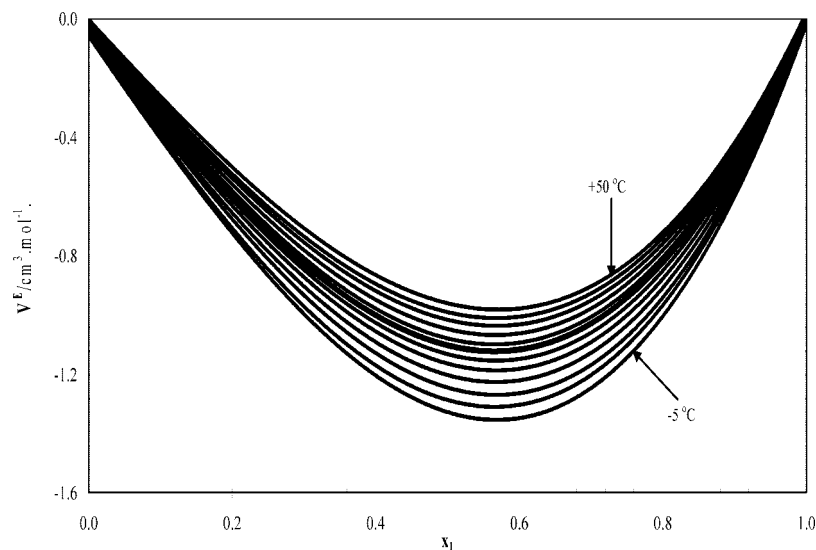


Figure 3. Excess molar volume,  $V^E$ , plotted against water mole fraction,  $x_1$ , for the aqueous mixtures of ethanol.

Table 3. Excess Molar Volume ( $V^E/\text{cm}^3 \cdot \text{mol}^{-1}$ ) for the Aqueous Mixtures of Ethanol at Different Temperatures and Water Mole Fractions ( $x_1$ )<sup>a</sup>

temp °C	$x_1$								
	0.9	0.8	0.7	0.6	0.5	0.4	0.3	0.2	0.1
-5	-0.601	-0.938	-1.287	-1.340	-1.236	-1.087	-0.937	-0.724	-0.417
0	-0.586	-0.913	-1.234	-1.292	-1.198	-1.065	-0.911	-0.703	-0.393
5	-0.561	-0.892	-1.186	-1.259	-1.164	-1.027	-0.866	-0.666	-0.377
10	-0.542	-0.860	-1.154	-1.211	-1.111	-0.986	-0.844	-0.654	-0.355
15	-0.504	-0.839	-1.121	-1.156	-1.087	-0.952	-0.812	-0.624	-0.332
20	-0.470	-0.823	-1.081	-1.125	-1.052	-0.929	-0.793	-0.607	-0.296
25	-0.443(-0.454)	-0.812	-1.041	-1.093(-1.096)	-1.019	-0.907	-0.780	-0.486	-0.281(-0.267)
30	-0.407	-0.797	-1.018	-1.068	-1.001	-0.888	-0.763	-0.563	-0.252
35	-0.384	-0.779	-0.987	-1.035	-0.970	-0.859	-0.740	-0.541	-0.229
40	-0.363	-0.753	-0.962	-1.009	-0.934	-0.842	-0.702	-0.520	-0.214
45	-0.348	-0.737	-0.934	-0.981	-0.906	-0.826	-0.687	-0.493	-0.205
50	-0.335	-0.714	-0.914	-0.949	-0.879	-0.799	-0.661	-0.465	-0.183

<sup>a</sup> Some literature values are also given in parentheses.

Table 4. Values of  $(-\beta \cdot 10^4 / ^\circ\text{C}^{-1})$  as Determined from  $\rho(t) = \rho(25) \cdot e^{\beta(t-25)}$  for the System (LiCl + Water + Ethanol) with  $x_1$  and  $m$  Being Water Mole Fraction in the Solvent Mixture and LiCl Aquamolality, Respectively<sup>a</sup>

$m$	$x_1$										
	1.0	0.9	0.8	0.7	0.6	0.5	0.4	0.3	0.2	0.1	0.0
0.0	2.71	6.89	7.70	9.69	10.37	10.67	10.76	11.01	11.42	11.5	11.4
0.5	2.23	6.70	7.97	9.28	8.86	10.32	10.41	10.57	11.33	11.2	10.7
1.0	2.24	6.88	7.33	9.01	8.69	9.32	10.20	10.63	11.05	10.5	10.5
2.0	2.45	6.72	6.84	8.73	8.24	9.61	9.69	10.02	10.46	10.4	9.9
3.0	3.51	6.13	7.09	8.80	8.25	10.03	9.12	9.37	9.77	10.0	9.8
4.5	2.50	6.02	6.72	7.93	7.54	9.12	9.73	9.22	9.43	9.8	9.6
6.0	2.53	5.87	5.63	7.21	6.90	8.45	8.52	8.48	9.14	8.8	8.8
8.0	2.60	5.90	5.40	6.78	6.32	7.76	8.22	8.16	8.51	8.2	8.5
11.0	2.72	5.83	5.25	6.63	5.67	7.28	7.38	7.56	8.30	—	—
14.0	2.81	5.86	4.90	6.12	5.59	7.01	—	—	—	—	—
$\sigma$	3.01 (17.8)	5.50 (18.0)	4.82 (17.5)	5.91 (16.5)	5.52 (16.0)	6.80 (15.2)	6.42 (14.0)	7.40 (13.5)	8.02 (13.0)	8.4 (11.0)	8.2 (10.0)
	± 0.09	± 0.09	± 0.08	± 0.09	± 0.09	± 0.09	± 0.07	± 0.06	± 0.08	± 0.1	± 0.32

<sup>a</sup> Highest  $m$  values employed for the mixtures are given in parentheses, and the corresponding standard deviations ( $\sigma$ ) of the  $\beta$ -values are given at the bottom of each column.

viscometers were standardized using 20 °C literature values<sup>1,45</sup> of water (1.002), nitrobenzene (1.980), and aniline (4.467 mPa·s). Viscosities of the references were also measured from time to time as a check. For still higher viscosities, a previously measured solution served as the reference for the next one. For each measurement, the flow time taken was an average of at least three runs, and the time could be read with an estimated uncertainty within  $\pm 0.02$  s. The maximum uncertainties in the viscosity measurements (as could be estimated from the 20 °C reported data of the solvent mixtures<sup>1</sup>) are within  $\pm 1$  %.

**Electrical Conductivity Measurement.** A CyberScan CON500 conductivity meter from Eutech Instruments, Singapore (with reported resolution of 0.05 % and inaccuracy within  $\pm 1$  % of the given full scale), served to measure electrical conductivity. The conductivity meter was equipped with a thermal sensor along with provision of an automatic compensation for temperature variation. The  $\kappa$  values were directly measured employing any one of the five scales of the instrument covering the range from  $1 \mu\text{S} \cdot \text{cm}^{-1}$  to  $199.9 \text{mS} \cdot \text{cm}^{-1}$  (also the maximum readable value). Although

**Table 5. Viscosities ( $\eta/\text{mPa}\cdot\text{s}$ ) at Different Temperatures and LiCl Aquamolalities ( $m$ ) in Binary Mixtures of Water (1) and Ethanol (2) Having Mole Fractions  $x_1$  and  $x_2$** 

concentration $m$	temperature, $t/^\circ\text{C}$											
	-5	0	5	10	15	20	25	30	35	40	45	50
$x_1 = 1.0, x_2 = 0.0$												
0.0	—	—	1.519	1.308	1.140	1.005	0.894	0.799	0.723	0.655	0.599	0.548
0.5	2.273	1.944	1.663	1.424	1.243	1.087	0.970	0.866	0.782	0.722	0.668	0.625
1.0	2.554	2.107	1.784	1.518	1.346	1.160	1.052	0.929	0.834	0.774	0.714	0.665
2.0	2.831	2.370	2.000	1.701	1.502	1.308	1.165	1.047	0.941	0.866	0.802	0.747
3.0	3.191	2.681	2.266	1.936	1.729	1.495	1.339	1.239	1.083	0.977	0.910	0.859
4.5	3.649	3.133	2.690	2.303	2.034	1.777	1.586	1.422	1.280	1.177	1.076	1.003
6.0	4.461	3.815	3.258	2.777	2.452	2.131	1.906	1.713	1.532	1.406	1.293	1.194
8.0	6.735	5.744	4.899	4.170	3.602	3.199	2.800	2.486	2.256	2.071	1.919	1.742
11.0	10.848	9.191	7.784	6.579	5.630	4.898	4.292	3.812	3.407	3.091	2.869	2.690
14.0	18.985	15.816	13.169	10.970	9.142	7.966	6.899	6.073	5.332	4.812	4.412	4.123
17.8	28.660	24.988	21.788	19.662	17.145	14.889	12.680	11.538	10.462	9.741	8.984	8.265
$x_1 = 0.9, x_2 = 0.1$												
0.0	6.025	4.997	4.089	3.340	2.706	2.268	1.920	1.656	1.448	1.271	1.121	0.975
0.5	6.601	5.372	4.406	3.614	2.924	2.473	2.090	1.811	1.551	1.361	1.185	1.041
1.0	7.317	5.872	4.703	3.852	3.181	2.652	2.247	1.950	1.708	1.459	1.288	1.115
2.0	7.802	6.321	5.118	4.196	3.425	2.875	2.569	2.094	1.809	1.533	1.369	1.203
3.0	8.355	6.895	5.751	4.695	3.832	3.207	2.744	2.352	1.985	1.669	1.472	1.296
4.5	10.453	8.678	7.206	5.853	5.086	4.261	3.707	3.207	2.852	2.506	2.315	2.048
6.0	11.283	9.824	8.554	7.283	6.125	5.115	4.387	3.864	3.372	3.075	2.879	2.492
8.0	17.824	14.459	11.724	9.516	7.844	6.608	5.629	5.221	4.252	3.750	3.429	3.154
11.0	33.686	26.232	20.525	16.479	12.406	10.551	8.894	7.648	6.640	5.833	5.280	4.782
14.0	60.400	46.020	35.471	27.642	20.615	17.491	14.560	12.697	11.231	9.266	8.272	7.470
18.0	115.642	88.450	67.556	51.851	37.369	31.211	25.390	21.732	18.914	15.286	13.943	12.183
$x_1 = 0.8, x_2 = 0.2$												
0.0	7.549	6.169	5.037	4.102	3.433	2.841	2.450	2.101	1.772	1.557	1.369	1.202
0.5	8.076	6.618	5.425	4.471	3.704	3.085	2.595	2.257	1.907	1.605	1.437	1.285
1.0	8.690	7.115	5.839	4.821	4.038	3.400	2.744	2.392	2.072	1.761	1.532	1.314
2.0	9.689	7.892	6.501	5.256	4.342	3.634	3.068	2.601	2.251	1.901	1.691	1.438
3.0	13.300	10.558	8.398	6.656	5.348	4.466	3.759	3.238	2.793	2.460	2.156	1.924
4.5	15.579	12.442	9.976	7.943	6.425	5.380	4.546	3.915	3.323	2.936	2.498	2.185
6.0	20.010	15.577	12.128	9.704	7.872	6.598	5.565	4.805	4.115	3.582	3.135	2.701
8.0	29.226	22.508	17.425	13.738	10.239	8.634	7.305	6.609	5.419	4.759	4.201	3.787
11.0	50.673	38.717	29.934	23.195	17.380	14.550	12.092	10.332	8.820	7.707	6.782	6.157
14.0	93.315	69.558	52.975	40.751	29.682	24.752	20.307	17.455	15.191	12.407	11.300	9.624
17.5	184.015	137.485	102.739	76.793	54.108	42.847	35.508	29.811	25.788	20.559	18.467	15.922
$x_1 = 0.7, x_2 = 0.3$												
0.0	7.172	5.947	4.933	4.093	3.372	2.842	2.350	2.040	1.780	1.560	1.371	1.170
0.5	7.668	6.365	5.428	4.487	3.632	3.051	2.610	2.234	1.935	1.669	1.435	1.251
1.0	8.276	6.898	5.778	4.759	3.928	3.217	2.738	2.395	2.019	1.724	1.539	1.361
2.0	9.651	7.889	6.554	5.341	4.340	3.653	3.134	2.720	2.321	1.975	1.695	1.523
3.0	13.241	10.698	8.599	6.926	5.683	4.765	4.114	3.582	3.002	2.641	2.319	1.975
4.5	16.264	13.142	10.598	8.468	6.918	5.826	4.941	4.270	3.671	3.189	2.791	2.413
6.0	20.370	16.269	13.050	10.400	8.486	7.137	6.003	5.108	4.502	3.921	3.435	2.980
8.0	32.411	25.185	19.554	15.375	11.527	9.708	8.265	7.143	6.157	5.419	4.832	4.174
11.0	57.668	46.354	34.910	27.140	20.262	17.087	14.171	12.292	10.841	8.913	7.857	7.000
14.0	128.627	96.395	72.165	54.823	39.567	32.693	26.659	22.650	19.673	15.779	14.234	12.361
16.5	214.294	159.709	119.043	88.746	62.740	51.068	40.735	34.304	29.270	23.151	20.749	17.691
$x_1 = 0.6, x_2 = 0.4$												
0.0	5.931	4.978	4.176	3.499	2.922	2.463	2.089	1.812	1.582	1.430	1.270	1.140
0.5	6.377	5.358	4.497	3.767	3.127	2.641	2.250	1.953	1.706	1.492	1.341	1.186
1.0	6.889	5.819	4.841	4.046	3.379	2.838	2.419	2.100	1.825	1.591	1.423	1.255
2.0	7.975	6.711	5.621	4.660	3.896	3.275	2.794	2.420	2.108	1.803	1.610	1.421
3.0	11.736	9.552	7.769	6.321	5.182	4.367	3.708	3.191	2.760	2.422	2.185	1.964
4.5	15.485	12.347	9.834	8.011	6.568	5.551	4.691	4.063	3.495	3.074	2.770	2.490
6.0	21.833	17.208	13.529	10.918	8.530	7.378	6.146	5.070	4.368	3.820	3.497	3.059
8.0	32.700	25.512	19.860	15.586	11.686	10.045	8.413	7.227	6.210	5.454	4.902	4.289
11.0	66.130	50.701	38.662	29.881	22.074	18.596	15.216	13.179	11.672	9.429	8.456	7.319
14.0	147.813	111.617	84.103	63.494	45.490	37.249	30.118	25.190	22.061	17.464	15.544	13.483
16.0	300.611	222.805	165.149	122.426	84.843	69.094	54.459	44.644	37.475	29.651	26.232	22.153
$x_1 = 0.5, x_2 = 0.5$												
0.0	4.829	4.123	3.518	2.995	2.539	2.153	1.840	1.598	1.407	1.270	1.140	1.020
0.5	5.148	4.441	3.829	3.262	2.755	2.340	2.007	1.754	1.541	1.348	1.211	1.074
1.0	5.821	4.915	4.158	3.527	2.980	2.571	2.191	1.947	1.733	1.476	1.341	1.148
2.0	6.835	5.771	4.947	4.119	3.487	2.934	2.530	2.214	1.939	1.711	1.529	1.358
3.0	10.402	8.541	7.012	5.753	4.755	4.065	3.463	3.011	2.606	2.312	2.082	1.724
4.5	13.961	11.341	9.199	7.473	6.242	5.300	4.516	3.878	3.391	2.971	2.613	2.300

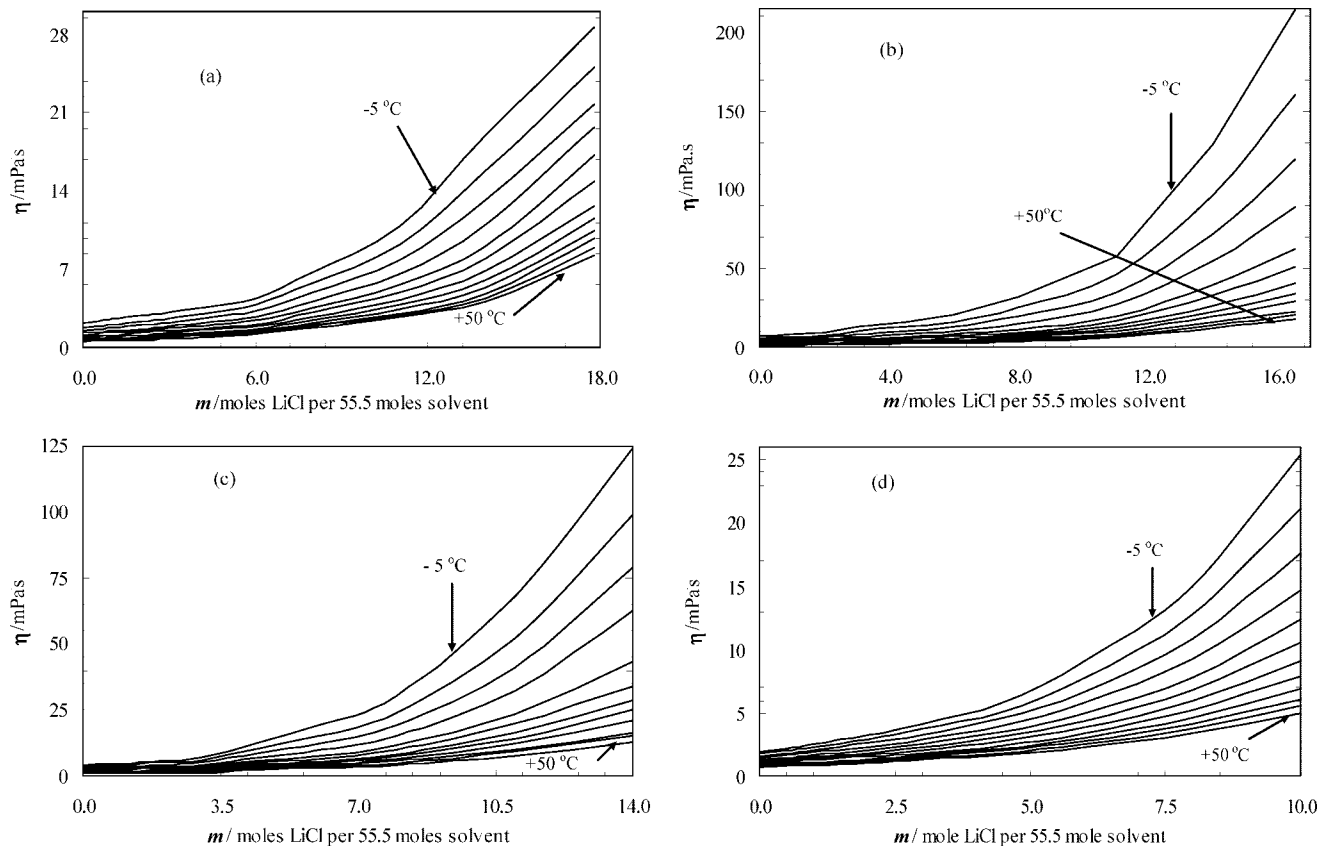
Table 5 Continued

concentration <i>m</i>	temperature, <i>t</i> /°C											
	-5	0	5	10	15	20	25	30	35	40	45	50
6.0	20.305	15.899	12.727	10.234	7.997	6.692	5.985	4.930	4.262	3.752	3.366	2.911
8.0	31.501	24.866	19.598	15.599	12.519	10.103	8.447	7.266	6.180	5.454	4.866	4.184
11.0	79.870	60.159	46.474	35.686	26.401	21.962	18.209	15.734	13.743	10.983	10.021	8.455
14.0	180.863	132.010	95.569	71.990	51.472	41.370	33.179	28.115	24.131	19.012	16.993	14.556
15.2	333.404	245.142	180.224	134.336	93.211	75.946	60.253	49.001	41.068	32.397	28.465	22.821
$x_1 = 0.4, x_2 = 0.6$												
0.0	3.991	3.451	2.980	2.570	2.212	1.901	1.651	1.446	1.296	1.149	1.039	0.932
0.5	4.501	3.955	3.349	2.837	2.429	2.090	1.818	1.609	1.444	1.271	1.126	1.006
1.0	4.921	4.211	3.625	3.113	2.638	2.284	2.010	1.755	1.505	1.325	1.217	1.100
2.0	5.811	5.020	4.285	3.653	3.152	2.692	2.331	2.019	1.795	1.575	1.367	1.251
3.0	6.959	6.001	5.115	4.354	3.713	3.187	2.755	2.336	2.145	1.887	1.622	1.435
4.5	12.770	10.499	8.686	7.138	5.880	5.087	4.409	3.833	3.347	2.931	2.629	2.352
6.0	19.116	15.185	12.106	9.770	7.715	6.536	5.546	4.832	4.199	3.691	3.299	2.902
8.0	30.193	24.008	19.051	15.238	11.601	9.930	8.460	7.339	6.312	5.565	4.936	4.313
11.0	67.538	52.155	40.710	31.932	23.587	19.735	16.242	14.135	12.430	10.129	9.193	7.865
14.0	123.648	98.860	78.949	62.320	43.351	33.894	28.536	24.844	21.169	16.393	14.945	12.853
$x_1 = 0.3, x_2 = 0.7$												
0.0	3.345	2.938	2.579	2.260	1.980	1.715	1.513	1.356	1.215	1.096	0.998	0.902
0.5	3.741	3.357	2.874	2.513	2.194	1.902	1.686	1.498	1.331	1.181	1.072	0.982
1.0	4.194	3.635	3.173	2.751	2.457	2.126	1.849	1.621	1.489	1.311	1.175	1.035
2.0	5.009	4.390	3.799	3.286	2.843	2.469	2.165	1.932	1.726	1.521	1.389	1.239
3.0	6.100	5.381	4.631	3.996	3.400	2.954	2.594	2.302	2.045	1.822	1.675	1.469
4.5	9.056	7.495	6.206	5.238	4.486	3.877	3.363	2.996	2.639	2.362	2.157	1.798
6.0	12.910	10.622	8.726	7.178	5.920	5.127	4.449	3.873	3.387	2.985	2.702	2.492
8.0	22.497	18.653	15.460	12.816	10.651	9.067	7.704	6.684	5.764	5.118	4.594	4.180
11.0	67.128	52.393	40.820	32.134	23.727	19.960	16.605	14.327	12.652	10.269	9.301	8.108
13.5	139.112	104.463	78.306	59.415	42.780	35.153	28.478	24.163	20.882	16.555	14.885	12.766
$x_1 = 0.2, x_2 = 0.8$												
0.0	2.805	2.491	2.210	1.959	1.721	1.515	1.353	1.218	1.110	1.004	0.925	0.839
0.5	3.126	2.787	2.485	2.213	1.939	1.709	1.521	1.358	1.223	1.105	1.015	0.925
1.0	3.529	3.120	2.763	2.435	2.125	1.869	1.654	1.489	1.345	1.208	1.103	1.007
2.0	4.411	3.852	3.360	2.925	2.524	2.254	2.003	1.794	1.602	1.420	1.328	1.225
3.0	5.248	4.613	4.054	3.554	3.100	2.703	2.381	2.130	1.925	1.714	1.564	1.420
4.5	7.139	6.237	5.448	4.748	4.119	3.574	3.131	2.789	2.487	2.252	2.072	1.823
6.0	11.375	9.575	8.021	6.713	5.598	4.830	4.237	3.728	3.259	2.955	2.691	2.514
8.0	16.025	13.729	11.165	8.999	7.965	7.070	6.265	5.506	4.765	4.077	3.569	3.101
11.0	63.702	49.786	39.279	30.949	23.481	19.622	16.284	14.187	12.501	10.199	9.135	7.575
13.0	123.911	91.252	69.106	53.332	38.717	31.596	26.141	22.233	19.276	15.356	13.709	11.483
$x_1 = 0.1, x_2 = 0.9$												
0.0	2.307	2.059	1.837	1.639	1.510	1.355	1.249	1.156	1.067	0.920	0.860	0.760
0.5	2.871	2.595	2.386	2.149	1.887	1.710	1.537	1.393	1.291	1.158	1.074	0.991
1.0	3.245	2.918	2.615	2.340	2.096	1.892	1.690	1.546	1.408	1.285	1.189	1.095
2.0	3.911	3.512	3.150	2.822	2.503	2.233	2.005	1.817	1.673	1.530	1.413	1.295
3.0	4.839	4.313	3.842	3.423	3.047	2.684	2.399	2.176	1.980	1.796	1.662	1.521
4.5	6.701	5.883	5.166	4.529	3.950	3.496	3.103	2.820	2.529	2.287	2.133	1.909
6.0	10.288	8.711	7.372	6.334	5.456	4.771	4.290	3.792	3.335	3.034	2.790	2.608
8.0	16.193	13.643	11.483	9.681	8.225	7.103	6.253	5.524	4.879	4.342	3.992	3.687
11.0	86.485	68.040	53.466	41.529	31.392	26.382	21.428	18.652	16.420	13.181	12.033	10.423
$x_1 = 0.0, x_2 = 1.0$												
0.0	1.975	1.775	1.629	1.468	1.341	1.207	1.105	1.010	0.920	0.840	0.772	0.713
0.5	2.208	2.043	1.863	1.695	1.495	1.357	1.218	1.089	1.006	0.928	0.866	0.807
1.0	2.546	2.313	2.099	1.908	1.715	1.524	1.412	1.306	1.129	1.046	0.968	0.884
2.0	3.283	2.943	2.638	2.366	2.100	1.869	1.677	1.527	1.369	1.267	1.164	1.070
3.0	4.167	3.722	3.323	2.959	2.603	2.307	2.057	1.846	1.671	1.524	1.414	1.285
4.5	5.819	5.158	4.570	4.045	3.546	3.124	2.767	2.469	2.223	2.010	1.842	1.677
6.0	9.082	7.821	6.735	5.802	4.988	4.395	3.869	3.436	3.077	2.762	2.538	2.335
8.0	14.963	12.709	10.782	9.203	7.807	6.784	5.908	5.171	4.578	4.089	3.735	3.437
10.0	25.437	21.163	17.617	14.676	12.335	10.561	9.071	7.924	6.884	6.076	5.603	5.009

different options of cell constants were available, for uniformity sake, the cell of  $1 \text{ cm}^{-1}$  was employed throughout. The instrument was first calibrated at  $25 \text{ }^\circ\text{C}$  with standard aqueous KCl solutions,<sup>1</sup> and the calibration was also monitored from time to time during the experimentation. Previously reported<sup>46</sup> values for concentrated aqueous solutions

of  $\text{Na}_2\text{SO}_4$  at different temperatures could well be reproduced within  $\pm 0.04 \%$ . For the conductivity measurement, equal portions of the sample, taken in two identical narrow-necked cells, were first thermostatted in a bath of required temperature for about 20 min. One of them served for the conductivity measurement, while the ASTM-calibrated ther-

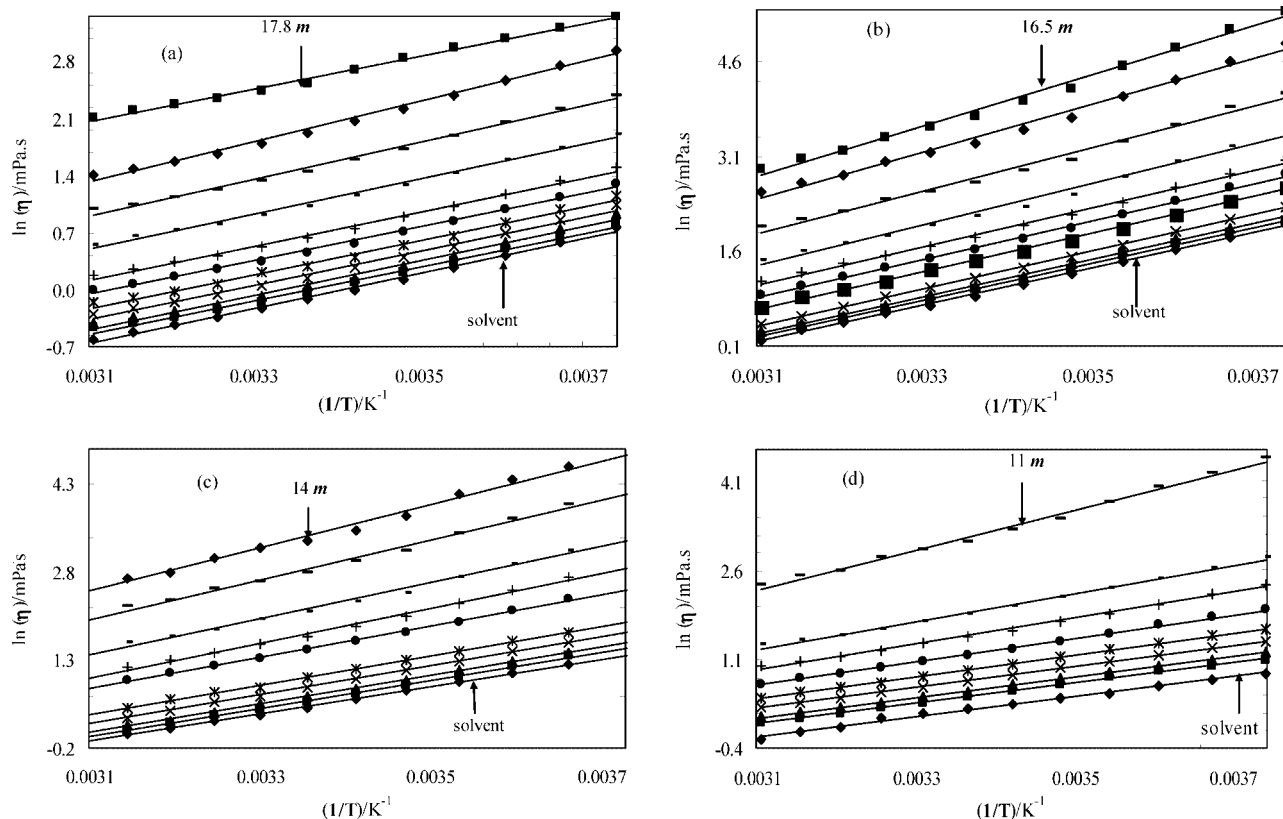




**Figure 4.** (a–d) Viscosity,  $\eta$ , fitted to LiCl aquamolality,  $m$ , in the isotherm  $\eta(m) = \eta^{\circ} + a_1 \cdot m + a_2 \cdot m^2$  from  $-5^{\circ}\text{C}$  to  $+50^{\circ}\text{C}$  at  $5^{\circ}\text{C}$  intervals. The binary ethanol mixtures of water mole fractions,  $x_1$ ;  $\eta^{\circ}$  refers to viscosity of the solvent mixtures (refer to Table 1) (a)  $x_1 = 1.0$ , (b)  $x_1 = 0.7$ , (c)  $x_1 = 0.4$ , and (d)  $x_1 = 0.0$ .

**Table 6.** Coefficients (in Appropriate Units) of the Polynomial  $\eta/\eta^{\circ} = 1 + B \cdot m + C \cdot m^2 + D \cdot m^3$  at Different Temperatures in Aqueous Mixtures of Ethanol of Various Water Mole Fractions  $x_1$  (Other Details in the Text)

$x_1$	parameters	temperature, $t/^{\circ}\text{C}$											
		-5	0	5	10	15	20	25	30	35	40	45	50
0.0	B	0.347	0.345	0.325	0.317	0.291	0.270	0.252	0.253	0.245	0.234	0.249	0.239
	C	-0.029	-0.026	-0.021	-0.017	-0.014	-0.007	-0.004	-0.006	-0.002	-0.002	-0.004	-0.002
	D	0.011	0.010	0.009	0.008	0.007	0.006	0.005	0.005	0.004	0.004	0.004	0.003
0.1	B	2.026	1.799	1.605	1.411	1.123	1.063	0.898	0.849	0.826	0.797	0.777	0.760
	C	-0.771	-0.667	-0.577	-0.487	-0.369	-0.343	-0.278	-0.261	-0.254	-0.222	-0.216	-0.198
	D	0.080	0.070	0.060	0.051	0.039	0.036	0.030	0.028	0.027	0.024	0.023	0.021
0.2	B	1.263	0.927	0.753	0.668	0.498	0.429	0.399	0.352	0.321	0.292	0.304	0.333
	C	-0.433	-0.304	-0.236	-0.200	-0.131	-0.104	-0.090	-0.074	-0.066	-0.051	-0.055	-0.058
	D	0.045	0.034	0.028	0.023	0.017	0.015	0.013	0.012	0.011	0.009	0.009	0.008
0.3	B	0.802	0.626	0.472	0.363	0.300	0.267	0.229	0.204	0.177	0.147	0.145	0.098
	C	-0.251	-0.185	-0.129	-0.088	-0.057	-0.044	-0.030	-0.022	-0.015	-0.001	-0.001	-0.016
	D	0.031	0.024	0.019	0.015	0.011	0.010	0.008	0.007	0.007	0.005	0.005	0.008
0.4	B	0.223	0.284	0.331	0.337	0.267	0.211	0.225	0.249	0.202	0.161	0.161	0.181
	C	-0.013	-0.019	-0.038	-0.042	-0.019	-0.009	-0.001	-0.007	-0.004	-0.022	-0.021	-0.014
	D	0.027	0.010	0.010	0.010	0.007	0.006	0.005	0.005	0.003	0.002	0.003	0.003
0.5	B	2.322	2.020	1.738	1.508	1.211	1.178	1.087	0.938	0.843	0.770	0.706	0.558
	C	-0.641	-0.549	-0.461	-0.394	-0.303	-0.292	-0.260	-0.219	-0.193	-0.169	-0.151	-0.112
	D	0.050	0.043	0.036	0.031	0.024	0.023	0.021	0.018	0.017	0.014	0.013	0.011
0.6	B	0.486	0.416	0.400	0.342	0.312	0.282	0.283	0.262	0.215	0.207	0.193	0.167
	C	-0.096	-0.076	-0.072	-0.057	-0.047	-0.038	-0.033	-0.027	-0.017	-0.012	-0.010	-0.002
	D	0.011	0.009	0.008	0.007	0.006	0.005	0.005	0.004	0.004	0.003	0.003	0.003
0.7	B	0.481	0.412	0.398	0.340	0.312	0.282	0.283	0.262	0.216	0.210	0.201	0.180
	C	-0.096	-0.076	-0.072	-0.057	-0.047	-0.038	-0.033	-0.027	-0.017	-0.012	-0.011	-0.003
	D	0.010	0.009	0.008	0.007	0.006	0.005	0.005	0.004	0.004	0.003	0.003	0.003
0.8	B	0.362	0.347	0.310	0.274	0.234	0.197	0.193	0.184	0.186	0.200	0.186	0.200
	C	-0.055	-0.052	-0.044	-0.035	-0.026	-0.014	-0.015	-0.010	-0.011	-0.013	-0.011	-0.013
	D	0.006	0.006	0.005	0.004	0.003	0.003	0.003	0.002	0.003	0.002	0.003	0.003
0.9	B	0.197	0.185	0.179	0.153	0.181	0.171	0.215	0.192	0.169	0.157	0.153	0.152
	C	-0.017	-0.016	-0.014	-0.009	-0.010	-0.007	-0.015	-0.011	-0.008	-0.009	-0.009	-0.011
	D	0.003	0.003	0.003	0.003	0.002	0.002	0.002	0.002	0.002	0.002	0.002	0.002
1.0	B	0.092	0.154	0.209	0.199	0.194	0.228	0.245	0.280	0.290	0.287	0.099	0.154
	C	0.011	-0.006	-0.018	-0.016	-0.014	-0.022	-0.027	-0.035	-0.036	-0.034	-0.011	-0.006
	D	0.001	0.002	0.003	0.003	0.003	0.003	0.003	0.004	0.004	0.003	0.004	0.002



**Figure 5.** (a–d)  $\ln(\eta)$  vs  $1/T$  plots to determine flow activation energies ( $E_a$ ) of the LiCl solutions in aqueous ethanol of different water mole fractions,  $x_1$ : (a)  $x_1 = 1.0$ , (b)  $x_1 = 0.7$ , (c)  $x_1 = 0.4$ , and (d)  $x_1 = 0.1$ .

**Table 7.** Conductivity ( $E_c$ ) and Flow ( $E_a$ ) Activation Energies ( $\text{kJ}\cdot\text{mol}^{-1}$ ) for LiCl Solutions of Different Concentrations ( $m$ ) in Aqueous Mixtures of Ethanol Having Water Mole Fractions,  $x_1^a$

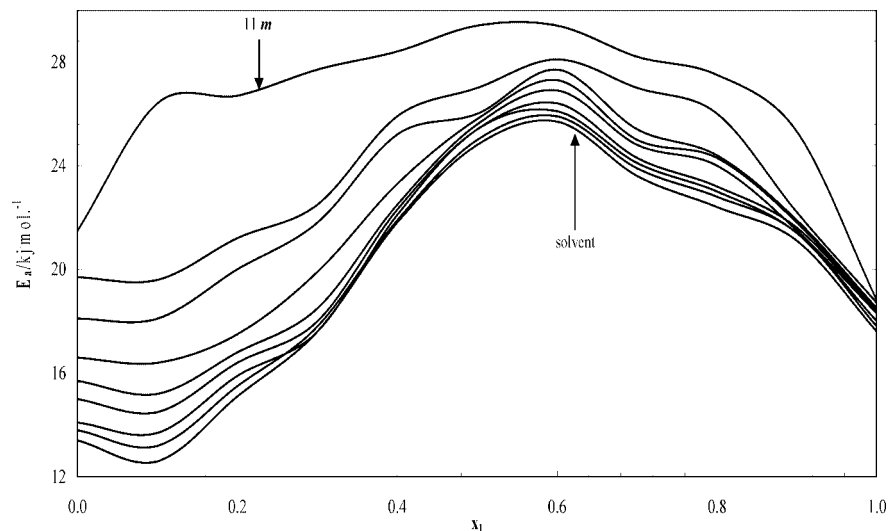
$x_1$	$E$ 's	aquamolality ( $m$ )									
		0.5	1.0	2.0	3.0	4.5	6.0	8.0	11.0	14.0	18.0
1.0	$E_c$	15.31	14.32	14.83	15.46	18.01	16.84	15.93	15.92	17.15	20.04 (17.8)
	$E_a$	17.91	18.12	18.30	18.72	18.98	19.24	19.49	19.74	20.58	21.35
0.9	$E_c$	19.63	20.67	19.80	19.58	19.07	18.87	19.07	19.83	21.50	24.16 (18.0)
	$E_a$	24.32	24.40	24.47	24.71	24.97	25.21	25.62	26.50	27.74	28.09
0.8	$E_c$	23.34	22.96	21.23	20.66	20.09	20.10	21.51	22.40	23.67	25.42 (17.5)
	$E_a$	24.50	24.73	25.01	25.36	25.58	25.81	26.82	27.91	29.47	31.50
0.7	$E_c$	21.74	20.91	20.63	20.51	20.41	20.52	22.05	21.68	25.18	26.85 (16.5)
	$E_a$	23.91	24.12	24.40	24.57	24.82	25.51	26.72	27.91	30.74	32.92
0.6	$E_c$	20.38	19.76	19.58	19.48	19.51	20.09	20.59	22.25	25.39	27.51 (16.0)
	$E_a$	22.33	22.61	22.88	23.73	24.02	25.89	26.61	28.72	31.63	34.51
0.5	$E_c$	20.02	18.71	18.25	18.70	18.61	18.48	20.54	22.66	25.56	26.63 (15.2)
	$E_a$	20.92	21.08	21.43	23.14	23.51	25.23	26.50	29.12	32.90	34.93
0.4	$E_c$	17.57	17.43	17.52	17.57	18.17	18.57	19.75	22.23	25.75 (14.0)	
	$E_a$	19.90	19.96	20.50	20.83	22.20	24.63	25.41	28.07	31.21	
0.3	$E_c$	16.96	16.25	16.39	16.72	17.38	18.32	19.61	22.50	26.61 (13.5)	
	$E_a$	17.97	18.31	18.50	18.90	20.52	21.81	22.50	27.82	31.30	
0.2	$E_c$	15.69	15.18	15.68	16.14	16.83	17.60	19.05	21.94	25.46 (13.0)	
	$E_a$	16.30	16.67	17.14	17.41	18.02	20.01	21.00	27.48	30.71	
0.1	$E_c$	15.93	14.10	14.82	15.34	16.50	17.43	18.95	23.86 (11.0)		
	$E_a$	14.42	14.81	15.66	16.31	17.05	18.91	20.20	27.32		
0.0	$E_c$	14.86	13.26	14.45	15.21	16.66	17.54	18.78	20.23 (10.0)		
	$E_a$	13.83	14.02	14.91	15.74	16.62	18.13	19.60	21.62		

<sup>a</sup> Values in parentheses correspond to the highest value of  $m$ .

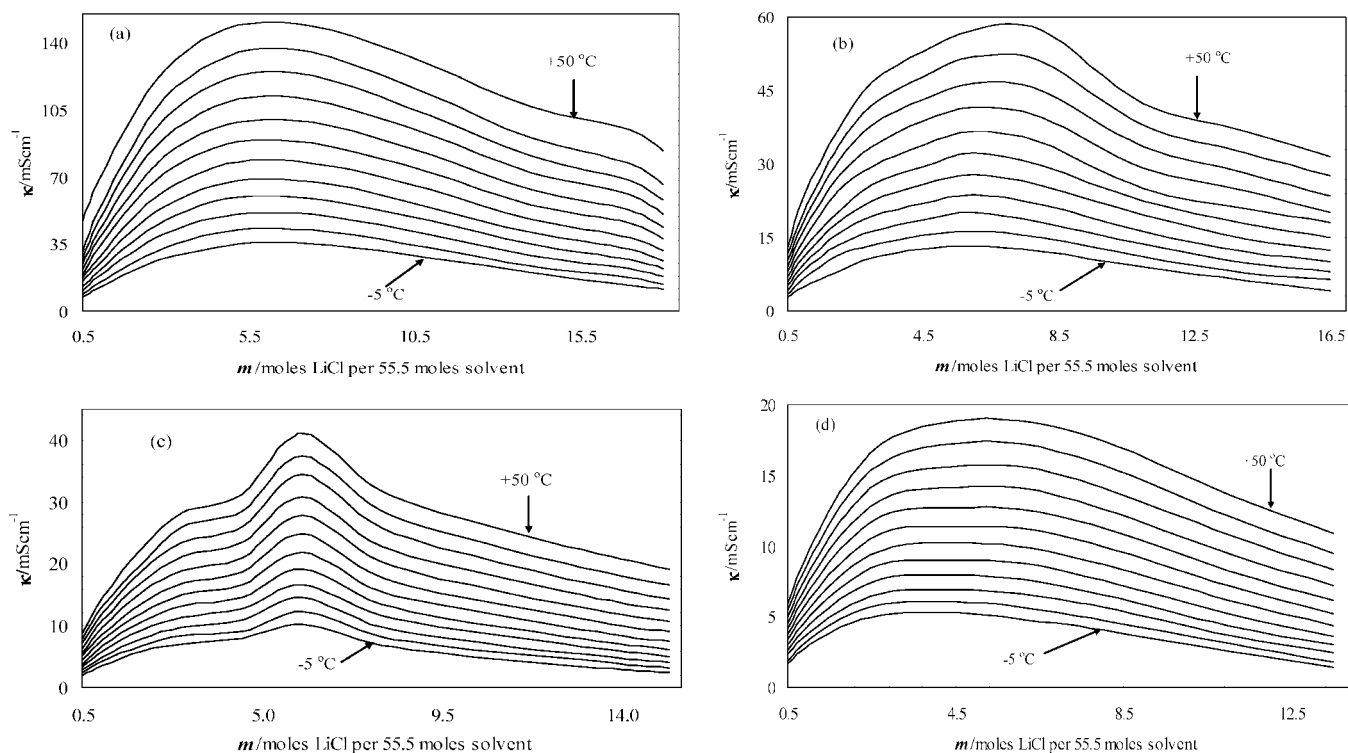
rometer was dipped in the other in such a way that positions of the electrode and thermometer were maintained each time. Subsequently, the mouths of the cells were closed with paraffin film to minimize any variation of the sample composition. Conductivity values could be reproduced within  $\pm 1\%$  for some randomly selected samples in the subsequent sessions.

## Results and Discussion

Table 1 presents density data for the solvent systems and their LiCl solutions, while the density isotherms at some selected compositions have been plotted against LiCl aquamolality ( $m$ ) in Figure 1a–d. Our measured densities (at 20 °C) for the mixtures ( $\rho^\circ$ ) and aqueous LiCl solutions fall



**Figure 6.** Variation trend of the flow activation energy ( $E_a$ ) with water mole fraction,  $x_1$ , in aqueous ethanol at different LiCl  $m$  (from bottom to top): 0.0, 0.5, 1.0, 2.0, 3.0, 4.5, 6.0, 8.0, and 11.0  $m$ .



**Figure 7.** (a–d) Electrical conductivity isotherms plotted against LiCl aquamolality ( $m$ ) in aqueous ethanol of different water mole fractions,  $x_1$ : (a)  $x_1 = 0.9$ , (b)  $x_1 = 0.7$ , (c)  $x_1 = 0.5$ , and (d)  $x_1 = 0.3$ .

within  $\pm 0.05\%$  of the corresponding literature values.<sup>1,2,40,47,48</sup> As expected, the density appreciably changed with both solvent composition and LiCl concentration. All the solutions exhibited almost a linear density increase with  $m$  making the  $\rho$ -isotherms fit a second order eq 1.

$$\rho(t, m) = d_0(t) + d_1(t) \cdot m + d_2(t) \cdot m^2 \quad (1)$$

where  $d_0$  is the fitted density of the neat solvent or mixture, whose values have deviated only up to 0.1% from the respective measured values,  $\rho_0$  (ref Table 1) and  $d_1$  and  $d_2$  are the corresponding density coefficients whose values are also listed in Table 2. A closer inspection of the plots suggests that change of density with LiCl concentration is greater when

water is in excess, but on the contrary, the variation with temperature (though minor) is more pronounced when ethanol is in excess. Since the concentration gradient  $g(x_1)$  of eq 1 does not appreciably change with temperature, it can be regarded as a specific parameter for a given solute–solvent system and can conveniently be used as a density index. Due to a negligible contribution of the term involving  $m^2$  for the system,  $g(x_1)$  can simply be compared with  $d_1$  of eq 1. The  $g$ -values (included in Table 1 and also plotted against the mixture compositions in Figure 2) can be employed for fairly accurate determination of solution density at any LiCl concentration and solvent composition within the given temperature range. Consequently, the density of the system

**Table 8. Electrical Conductivity ( $\kappa/\text{mS}\cdot\text{cm}^{-1}$ ) at Different Temperatures and LiCl Aquamolalities ( $m$ ) in Binary Mixtures of Water (1) and Ethanol (2) Having Mole Fractions  $x_1$  and  $x_2$** 

concentration aquamolality/ $m$	temperature, $t/^\circ\text{C}$											
	-5	0	5	10	15	20	25	30	35	40	45	50
	$x_1 = 1.0^a, x_2 = 0.0$											
0.5	—	—	26.100	29.900	33.500	37.400	41.500	45.800	49.900	54.300	58.500	62.800
1.0	—	—	46.400	52.000	58.700	65.300	72.900	80.000	87.000	94.500	102.200	110.100
2.0	—	—	76.400	86.100	96.200	107.400	120.400	132.000	144.200	156.400	168.300	180.800
3.0	—	—	95.900	109.600	122.600	137.100	152.400	166.800	181.900	197.400	<i>b</i>	<i>b</i>
4.5	—	—	114.800	130.000	144.600	160.800	176.800	194.200	<i>b</i>	<i>b</i>	<i>b</i>	<i>b</i>
6.0	—	—	120.400	136.200	152.300	168.900	186.600	<i>b</i>	<i>b</i>	<i>b</i>	<i>b</i>	<i>b</i>
8.0	—	—	115.300	130.700	146.100	162.700	179.500	197.300	<i>b</i>	<i>b</i>	<i>b</i>	<i>b</i>
11.0	—	—	93.700	106.900	120.800	135.600	151.000	167.000	182.600	199.700	<i>b</i>	<i>b</i>
14.0	—	—	69.900	80.100	90.900	103.600	117.000	131.100	145.400	160.400	175.400	191.400
17.8	—	—	47.100	55.200	64.500	74.400	85.000	96.100	108.600	122.600	136.400	150.600
	$x_1 = 0.9, x_2 = 0.1$											
0.5	7.340	9.020	10.980	13.140	15.340	17.840	19.200	21.800	24.550	27.300	30.400	33.100
1.0	12.120	14.820	17.950	21.040	24.550	28.050	33.200	37.650	42.100	47.400	52.500	57.400
2.0	20.800	25.300	30.400	36.100	41.800	48.200	55.200	61.900	69.800	77.600	85.300	93.500
3.0	27.600	33.500	40.300	47.500	55.100	63.000	72.400	81.300	90.700	100.600	111.600	122.200
4.5	33.300	40.700	48.600	57.300	65.900	74.800	85.100	95.600	107.000	118.700	130.100	143.300
6.0	36.100	43.200	51.200	60.000	69.100	78.900	89.300	100.500	112.600	124.900	137.600	150.300
8.0	34.500	41.100	49.300	57.500	66.500	75.900	85.800	96.800	108.600	120.800	133.000	146.100
11.0	28.000	33.500	40.200	47.300	54.400	63.300	72.500	81.700	92.000	102.200	113.000	125.500
14.0	20.100	24.000	29.100	35.100	41.000	48.100	55.500	63.400	72.300	81.500	90.600	101.000
18.0	11.620	14.480	18.030	22.100	26.700	32.000	37.800	44.200	51.100	58.300	66.100	74.400
	$x_1 = 0.8, x_2 = 0.2$											
0.5	3.300	4.220	5.240	6.380	7.650	9.040	10.53	12.11	13.79	15.53	17.35	19.23
1.0	6.210	8.000	9.830	11.91	14.21	16.70	19.38	22.40	25.40	28.70	32.00	35.30
2.0	10.54	15.04	18.30	21.60	26.20	29.50	33.80	37.70	42.50	47.10	51.80	57.00
3.0	13.76	19.25	23.90	28.40	32.70	37.50	42.40	47.80	53.50	59.50	64.70	70.90
4.5	16.85	23.70	29.80	32.70	39.40	44.40	50.60	56.70	63.40	70.00	76.90	83.50
6.0	17.93	26.80	32.00	36.60	42.80	48.90	55.70	62.20	69.50	76.80	84.40	91.80
8.0	15.30	20.00	24.30	28.90	34.10	40.70	45.60	52.00	58.60	65.50	73.20	80.20
11.0	11.62	14.64	17.86	21.20	25.30	29.70	34.60	39.70	45.20	51.10	57.10	63.60
14.0	8.940	11.38	14.05	17.05	20.20	24.00	28.10	32.60	37.50	42.70	48.30	54.30
17.5	6.700	8.680	10.90	13.42	16.31	19.58	23.00	27.20	31.30	36.20	41.10	46.50
	$x_1 = 0.7, x_2 = 0.3$											
0.5	2.790	3.480	4.220	5.070	5.970	6.950	8.000	9.090	10.32	11.61	12.91	14.30
1.0	4.900	6.820	8.240	9.670	11.13	12.80	14.59	16.45	18.34	20.30	23.60	25.60
2.0	8.040	11.28	13.39	15.67	18.18	20.20	24.60	27.30	30.50	33.60	36.90	40.50
3.0	10.97	13.56	16.34	19.32	22.40	25.90	29.60	33.70	38.00	42.20	46.70	51.20
4.5	12.61	15.40	18.60	22.00	25.80	29.60	34.00	38.90	43.20	47.90	52.90	58.60
6.0	13.12	16.39	20.30	23.90	27.90	32.30	36.70	41.60	46.50	51.90	57.40	63.20
8.0	12.11	14.96	18.08	21.60	25.50	29.80	34.50	39.60	45.10	51.00	57.30	64.00
11.0	9.100	11.18	13.72	16.42	19.57	22.40	25.20	29.10	33.50	37.90	42.40	47.40
14.0	6.170	7.840	9.860	12.12	14.82	17.76	21.00	24.50	28.20	32.30	36.70	41.40
16.5	4.180	6.500	8.140	10.13	12.47	15.07	18.08	20.10	23.60	27.60	31.50	36.00
	$x_1 = 0.6, x_2 = 0.4$											
0.5	2.390	2.880	3.440	4.060	4.750	5.470	6.250	7.100	7.960	8.890	9.850	10.83
1.0	4.150	5.070	6.050	7.090	8.240	9.490	10.82	12.22	13.69	15.25	16.87	17.62
2.0	6.830	8.290	9.960	11.63	13.48	15.50	17.58	19.84	22.10	24.50	27.10	29.60
3.0	8.460	10.19	12.23	14.33	16.60	19.07	21.60	24.40	27.00	30.10	33.00	36.30
4.5	9.840	11.84	14.20	16.60	19.30	22.10	25.10	28.20	31.40	35.10	38.70	42.40
6.0	9.850	12.02	14.30	16.85	19.72	22.70	25.80	29.20	32.80	36.60	40.40	44.60
8.0	8.670	10.55	12.77	15.08	17.69	20.00	23.00	26.20	29.60	33.30	37.20	41.00
11.0	6.770	8.100	9.890	11.91	14.22	16.65	19.37	21.80	25.00	28.40	32.00	35.80
14.0	4.100	5.160	6.570	8.100	9.780	11.72	13.95	16.43	19.08	21.30	24.50	27.90
16.0	3.030	3.870	5.030	6.290	7.730	9.400	11.34	13.44	15.81	18.46	21.10	24.10
	$x_1 = 0.5, x_2 = 0.5$											
0.5	2.120	2.510	2.970	3.450	3.990	4.560	5.160	5.800	6.500	7.220	8.010	8.800
1.0	3.630	4.300	5.100	5.940	6.780	7.710	8.720	9.790	10.92	12.12	13.34	14.58
2.0	5.830	6.890	8.060	9.360	10.76	12.16	13.76	15.44	17.23	19.02	20.10	22.70
3.0	7.060	8.410	9.900	11.46	13.18	15.00	16.94	19.00	21.20	23.50	26.00	28.30
4.5	7.940	9.250	10.91	12.70	14.67	16.64	18.84	20.98	23.50	26.00	28.60	31.40
6.0	10.39	12.37	14.51	16.77	19.27	21.90	24.90	27.90	30.90	34.40	37.50	41.20
8.0	6.830	8.210	9.830	11.54	13.45	15.61	17.84	20.30	22.90	25.70	28.60	31.70
11.0	4.650	5.690	6.930	8.370	9.920	11.64	13.51	15.52	17.80	20.10	22.70	25.50
14.0	3.030	3.790	4.730	5.860	7.110	8.520	10.11	11.85	13.73	15.87	18.15	20.70
15.2	2.570	3.250	4.170	5.090	6.230	7.550	9.030	10.71	12.59	14.47	16.67	19.13
	$x_1 = 0.4, x_2 = 0.6$											
0.5	1.980	2.290	2.650	3.060	3.470	3.910	4.390	4.910	5.440	5.990	6.570	7.180
1.0	3.340	3.850	4.480	5.140	5.830	6.590	7.380	8.220	9.100	10.02	11.00	11.98
2.0	5.160	6.020	6.950	7.970	9.090	10.25	11.52	12.84	14.24	15.68	17.18	18.74
3.0	6.160	7.220	8.360	9.600	10.93	12.35	13.85	15.48	17.17	18.91	20.70	22.60
4.5	6.770	7.940	9.300	10.70	12.27	13.83	15.60	17.48	19.47	21.60	23.70	26.10
6.0	6.550	7.700	8.990	10.46	12.03	13.69	15.49	17.35	19.38	21.40	23.60	26.00
8.0	5.530	6.560	7.750	9.080	10.54	12.11	13.79	15.61	17.58	19.64	21.70	23.90

Table 8 Continued

concentration aquamolality/ <i>m</i>	temperature, <i>t</i> /°C											
	-5	0	5	10	15	20	25	30	35	40	45	50
11.0	3.680	4.450	5.400	6.390	7.570	8.870	10.32	11.90	13.57	15.34	17.25	19.32
14.0	2.200	2.750	3.420	4.230	5.140	6.160	7.320	8.640	10.00	11.66	13.36	15.21
$x_1 = 0.3, x_2 = 0.7$												
0.5	1.691	1.933	2.380	2.690	3.030	3.400	3.780	4.170	4.590	5.030	5.500	5.950
1.0	2.990	3.420	3.910	4.450	5.010	5.590	6.230	6.900	7.600	8.290	9.000	9.780
2.0	4.520	5.200	5.920	6.740	7.600	8.510	9.470	10.52	11.56	12.68	13.80	15.01
3.0	5.210	5.990	6.870	7.830	8.870	9.940	11.20	12.41	13.61	14.93	16.33	17.75
4.5	5.290	6.020	6.920	7.960	9.030	10.19	11.41	12.74	14.16	15.68	17.29	18.90
6.0	4.860	5.700	6.640	7.680	8.790	9.990	11.27	12.64	14.13	15.62	17.22	18.88
8.0	4.070	4.760	5.660	6.560	7.580	8.710	9.940	11.27	12.63	14.13	15.70	17.40
11.0	2.560	3.090	3.710	4.400	5.240	6.150	7.160	8.260	9.460	10.78	12.17	13.63
13.5	1.460	1.830	2.440	2.990	3.640	4.360	5.210	6.140	7.200	8.300	9.500	10.87
$x_1 = 0.2, x_2 = 0.8$												
0.5	1.480	1.670	1.880	2.210	2.460	2.730	3.010	3.310	3.640	3.950	4.250	4.590
1.0	2.470	2.810	3.170	3.550	3.970	4.410	4.860	5.360	5.850	6.370	6.910	7.450
2.0	3.580	4.110	4.640	5.250	5.860	6.540	7.180	7.990	8.780	9.590	10.43	11.27
3.0	4.150	4.750	5.430	6.150	6.890	7.710	8.590	9.500	10.46	11.45	12.48	13.56
4.5	4.350	5.040	5.760	6.550	7.410	8.340	9.310	10.35	11.47	12.56	13.80	15.06
6.0	4.060	4.700	5.400	6.210	7.070	7.990	8.990	10.03	11.17	12.35	13.54	14.84
8.0	3.260	3.820	4.460	5.180	5.960	6.770	7.740	8.730	9.770	10.90	12.11	13.37
11.0	2.070	2.450	2.940	3.500	4.120	4.790	5.570	6.430	7.330	8.310	9.370	10.51
13.0	1.315	1.619	1.989	2.530	3.020	3.620	4.280	5.020	5.830	6.750	7.710	8.760
$x_1 = 0.1, x_2 = 0.9$												
0.5	1.305	1.461	1.644	1.821	2.300	2.510	2.740	2.980	3.230	3.500	3.760	4.040
1.0	2.410	2.710	3.030	3.390	3.730	4.110	4.510	4.930	5.360	5.790	6.240	6.690
2.0	3.310	3.750	4.210	4.710	5.240	5.820	6.430	7.050	7.670	8.350	9.010	9.710
3.0	3.780	4.260	4.820	5.430	6.040	6.720	7.440	8.200	9.000	9.780	10.66	11.56
4.5	3.820	4.360	4.960	5.610	6.340	7.200	7.970	8.830	9.770	10.69	11.70	12.75
6.0	3.510	4.030	4.650	5.341	6.030	6.830	7.660	8.530	9.510	10.49	11.58	12.68
8.0	2.740	3.210	3.760	4.310	4.950	5.660	6.440	7.280	8.120	9.090	10.07	11.17
11.0	1.527	1.890	2.560	3.020	3.540	4.120	4.760	5.540	6.310	7.190	8.070	9.110
$x_1 = 0.0, x_2 = 1.0$												
0.5	1.172	1.303	1.438	1.580	1.720	1.880	2.310	2.500	2.700	2.890	3.090	3.270
1.0	1.970	2.210	2.450	2.700	2.950	3.250	3.540	3.840	4.200	4.470	4.800	5.120
2.0	2.690	3.000	3.360	3.700	4.150	4.590	5.060	5.540	6.050	6.520	7.080	7.620
3.0	3.000	3.350	3.830	4.410	4.770	5.330	5.890	6.490	7.110	7.730	8.430	9.110
4.5	3.050	3.430	3.940	4.450	5.050	5.650	6.290	6.970	7.720	8.520	9.310	10.20
6.0	2.760	3.150	3.620	4.170	4.720	5.290	6.000	6.700	7.460	8.220	9.100	9.980
8.0	2.220	2.580	3.000	3.480	3.960	4.500	5.140	5.750	6.440	7.120	7.920	8.750
10.0	1.620	1.980	2.380	2.760	3.220	3.670	4.270	4.870	5.510	6.240	6.970	7.830

<sup>a</sup> Conductivities of the aqueous solutions at (-5 and 0) °C were not readable on the instrument due to fluctuations. <sup>b</sup> Values exceeded instrument's maximum range of 200 mS·cm<sup>-1</sup>.

can well be summarized as the following general expression

$$\rho(x_1, \mathbf{m}, t) = \rho_0(x_1, t) + \mathbf{g}(x_1) \cdot \mathbf{m} \quad (2)$$

Rapid increase of the  $\mathbf{g}$ -value on increasing  $x_1$  in water-rich solutions may be attributed to both preferential solvation by water molecules and its making compacter solvates.<sup>48</sup>

A rather useful thermodynamic property related to density of any solvent mixture is its excess molar volume,  $V^E(T)$ , which for binary mixtures may be expressed as

$$V^E = [(x_1 M_1 + x_2 M_2) / \rho] - [(x_1 M_1 / \rho_1) + (x_2 M_2 / \rho_2)] \quad (3)$$

where  $x_{1,2}$ ,  $M_{1,2}$ , and  $\rho_{1,2}$  are the mole fractions, molar masses, and densities of the two components (here water and ethanol, respectively), and  $\rho$  is the experimentally measured density of the mixture. Excess molar volume,  $V^E$ , of the mixture has been found to depend not only on its composition but also on temperature.  $V^E$  is an important quantity because it is a sensitive function of intermolecular interactions; therefore, its values for a given system should be measured over the entire composition and an extended temperature range.  $V^E$  for the mixture at

different temperatures and water mole fractions have been listed in Table 3, while  $V^E$  has been plotted against mixture composition at a series of temperatures in Figure 3. The  $V^E$  isotherms remain in the negative domain over the entire composition range and exhibit minima as well (the 25 °C plot in good agreement with the reported results<sup>47-49</sup>). Minima of all the  $V^E$  isotherms at the same water mole fraction of about 0.6 (Figure 3) suggest that temperature variation does not bring about any significant structural rearrangement in the solvent mixtures. The  $V^E$  values collected in Table 3 can be reproduced within 5 % at any desired water mole fraction ( $x_1$ ) and temperature ( $T/K$ ) by using the following expression

$$V^E(T) = [0.29 \pm 0.02 - (93 \pm 5)/T] + [1.56 \pm 0.09 - (1370 \pm 80)/T]x_1 + [-0.47 \pm 0.03 + (270 \pm 15)/T]x_1^2 + [-1.10 \pm 0.07 + (1110 \pm 70)/T]x_1^3 \quad (4)$$

Variation of volume with temperature is normally related to the thermal expansion coefficient,<sup>46</sup>  $\alpha(t) \equiv -d(\ln \rho)/dt$ . How-

**Table 9.** Coefficients (in Appropriate Units) of the Equation  $\kappa(T) = k_0 + k_1 \cdot m + k_2 \cdot m^2 + k_3 \cdot m^3$  at Different Temperatures in Binary Mixtures of Water (1) and Ethanol (2) Having Mole Fractions  $x_1$  and  $x_2$  ( $k_0$  Has Been Adjusted to Zero)

$k$ 's	temperature, $t/^\circ\text{C}$											
	-5	0	5	10	15	20	25	30	35	40	45	50
	$x_1 = 1.0, x_2 = 0.0$											
$k_1$	34.25	39.14	44.62	50.54	56.38	62.62	69.23	76.09	85.37	98.23	112.13	128.73
$k_2$	-3.64	-4.18	-4.78	-5.41	-6.03	-6.68	-7.38	-8.09	-9.14	-10.62	-12.22	-14.10
$k_3$	0.100	0.120	0.140	0.150	0.170	0.190	0.210	0.230	0.260	0.310	0.360	0.410
	$x_1 = 0.9, x_2 = 0.1$											
$k_1$	12.54	15.26	18.24	21.43	24.79	28.19	32.13	36.11	40.37	44.8	49.36	53.96
$k_2$	-1.29	-1.59	-1.90	-2.24	-2.60	-2.94	-3.36	-3.77	-4.21	-4.67	-5.15	-5.60
$k_3$	0.035	0.044	0.053	0.062	0.073	0.082	0.095	0.110	0.120	0.132	0.146	0.159
	$x_1 = 0.8, x_2 = 0.2$											
$k_1$	6.65	9.62	11.86	13.6	16.11	18.29	20.75	23.24	25.97	28.73	31.43	34.22
$k_2$	-0.76	-1.14	-1.42	-1.62	-1.92	-2.15	-2.44	-2.72	-3.03	-3.34	-3.63	-3.94
$k_3$	0.020	0.040	0.050	0.050	0.060	0.070	0.080	0.090	0.100	0.110	0.110	0.120
	$x_1 = 0.7, x_2 = 0.3$											
$k_1$	5.06	6.54	7.88	9.27	10.74	12.31	14.29	16.09	17.90	19.83	21.94	24.09
$k_2$	-0.57	-0.77	-0.92	-1.08	-1.24	-1.42	-1.66	-1.84	-2.04	-2.24	-2.47	-2.70
$k_3$	0.017	0.024	0.029	0.034	0.039	0.044	0.052	0.057	0.063	0.070	0.077	0.083
	$x_1 = 0.6, x_2 = 0.4$											
$k_1$	4.25	5.16	6.18	7.21	8.33	9.58	10.83	12.26	13.58	15.03	16.51	17.98
$k_2$	-0.53	-0.65	-0.78	-0.91	-1.04	-1.20	-1.35	-1.53	-1.68	-1.84	-2.01	-2.18
$k_3$	0.018	0.022	0.027	0.031	0.035	0.041	0.046	0.053	0.058	0.063	0.069	0.074
	$x_1 = 0.5, x_2 = 0.5$											
$k_1$	3.79	4.46	5.23	6.02	6.9	7.8	8.8	9.81	10.9	12.04	13.06	14.34
$k_2$	-0.49	-0.57	-0.66	-0.75	-0.86	-0.96	-1.08	-1.20	-1.33	-1.46	-1.56	-1.71
$k_3$	0.018	0.020	0.023	0.025	0.029	0.032	0.035	0.040	0.044	0.048	0.051	0.056
	$x_1 = 0.4, x_2 = 0.6$											
$k_1$	3.25	3.78	4.37	5.02	5.70	6.40	7.17	7.98	8.83	9.72	10.63	11.60
$k_2$	-0.45	-0.52	-0.59	-0.67	-0.76	-0.85	-0.95	-1.05	-1.15	-1.27	-1.38	-1.50
$k_3$	0.016	0.019	0.022	0.025	0.028	0.031	0.034	0.038	0.041	0.045	0.049	0.054
	$x_1 = 0.3, x_2 = 0.7$											
$k_1$	3.11	3.56	4.05	4.60	5.18	5.78	6.44	7.12	7.81	8.54	9.30	10.07
$k_2$	-0.52	-0.59	-0.66	-0.75	-0.84	-0.93	-1.03	-1.13	-1.23	-1.34	-1.44	-1.55
$k_3$	0.023	0.027	0.030	0.034	0.038	0.041	0.046	0.050	0.054	0.059	0.064	0.068
	$x_1 = 0.2, x_2 = 0.8$											
$k_1$	2.51	2.87	3.24	3.66	4.07	4.54	5.00	5.51	6.04	6.57	7.13	7.70
$k_2$	-0.42	-0.47	-0.53	-0.59	-0.65	-0.72	-0.78	-0.86	-0.94	-1.01	-1.09	-1.17
$k_3$	0.019	0.021	0.024	0.026	0.029	0.032	0.034	0.038	0.041	0.044	0.048	0.051
	$x_1 = 0.1, x_2 = 0.9$											
$k_1$	2.34	2.63	2.96	3.31	3.70	4.09	4.49	4.91	5.36	5.79	6.25	6.72
$k_2$	-0.40	-0.45	-0.50	-0.56	-0.62	-0.67	-0.73	-0.80	-0.86	-0.92	-0.98	-1.04
$k_3$	0.018	0.02	0.023	0.025	0.028	0.031	0.033	0.036	0.039	0.041	0.044	0.046
	$x_1 = 0.0, x_2 = 1.0$											
$k_1$	1.97	2.19	2.46	2.73	3.00	3.31	3.65	4.00	4.35	4.69	5.05	5.42
$k_2$	-0.36	-0.39	-0.44	-0.48	-0.52	-0.57	-0.62	-0.67	-0.73	-0.78	-0.83	-0.88
$k_3$	0.018	0.02	0.022	0.024	0.025	0.028	0.030	0.032	0.035	0.037	0.039	0.041

ever, a rather more useful empirical working expression proposed in this regard (at room temperature) is<sup>1,50</sup>

$$\rho(t) = \rho(25) \cdot e^{\beta(t-25)} \quad (5)$$

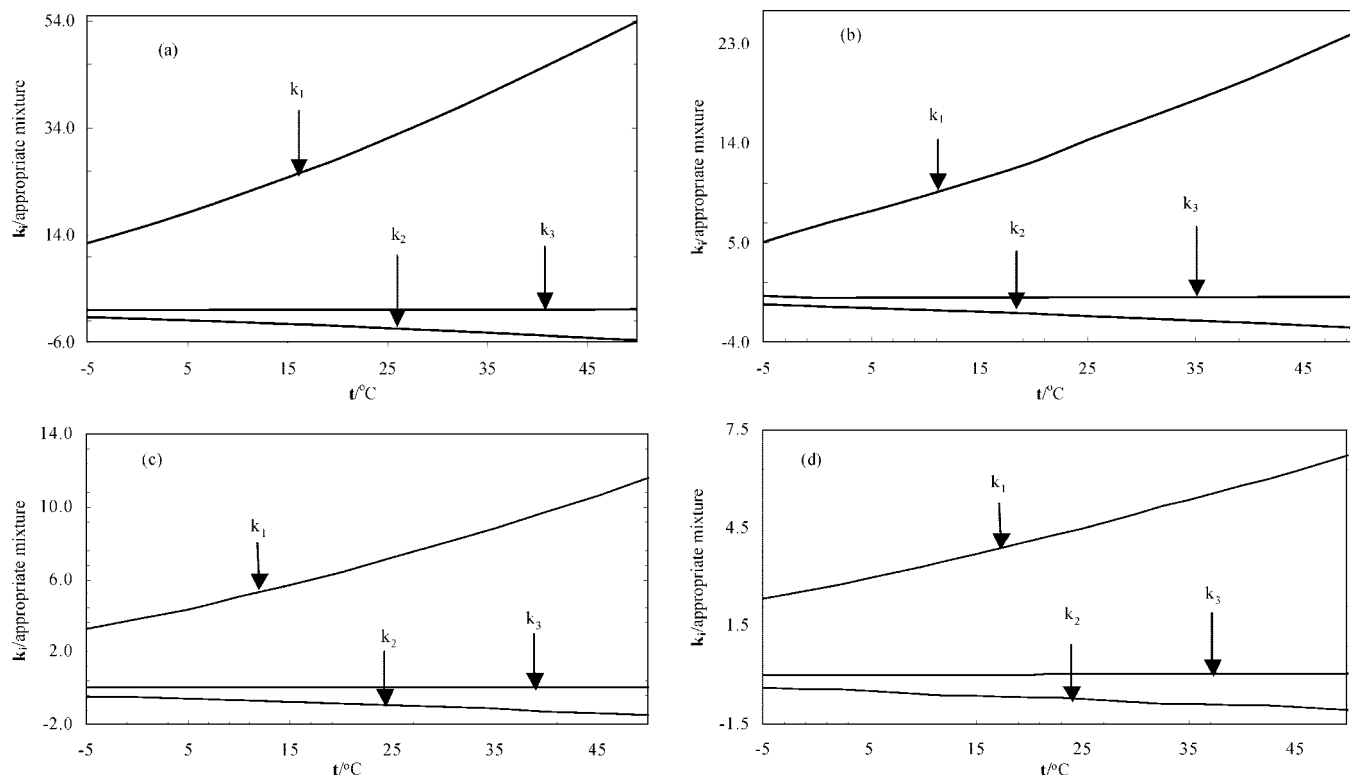
in which  $\rho(t)$  and  $\rho(25)$  are densities measured at  $t$  and  $25^\circ\text{C}$ , respectively. Parameter  $\beta$  (closely related to  $\alpha$ ) can be regarded as the temperature average coefficient of thermal expansion whose values for the entire system have been determined and collected in Table 4. The credibility of the  $\beta$ -values given in Table 4 may be judged from comparison of our determined value of  $-2.70 \cdot 10^{-4}$  per degree for water with the corresponding literature<sup>1</sup> value of  $-2.63 \cdot 10^{-4}$ .

Viscosities at a series of temperatures and LiCl aquamolalities ( $m$ ) are presented in Table 5 for each solvent mixture separately. Also the  $\eta$  values for some selected mixtures have been plotted as isotherms against LiCl concentration in Figure

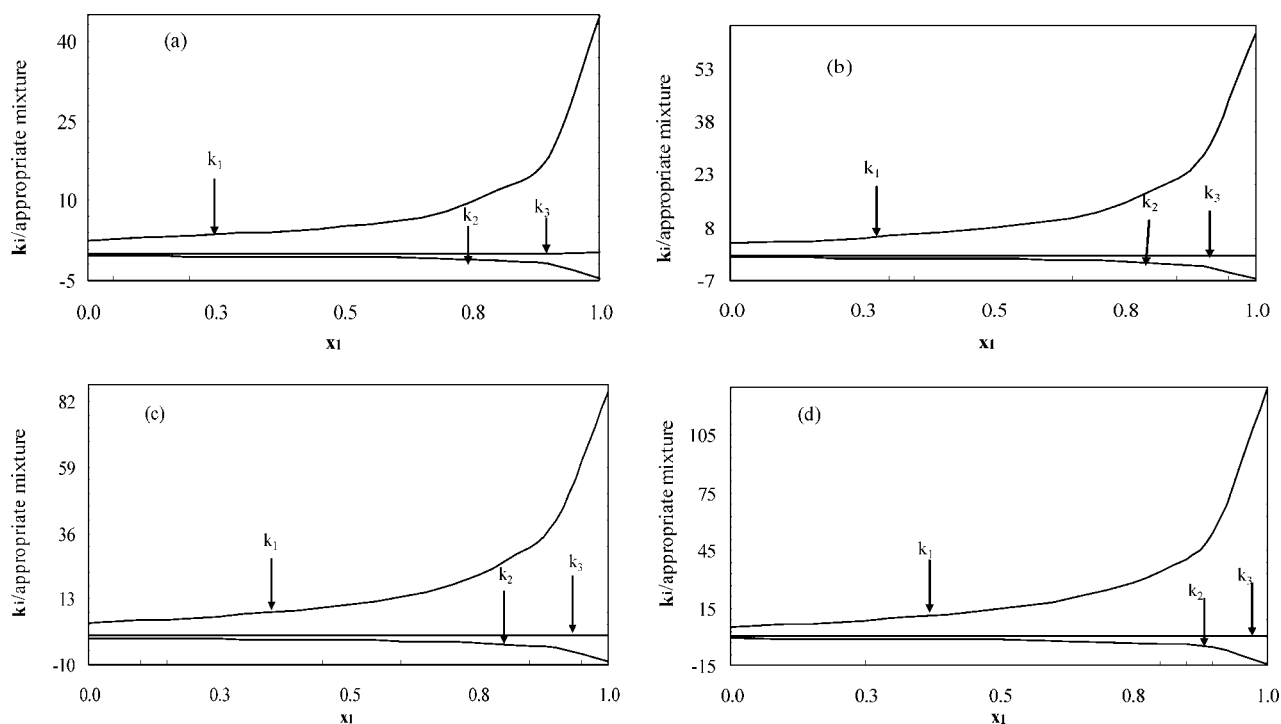
4a–d. The data fit very well to polynomials involving up to cubic terms in  $m$ . For the viscosity investigations, rather more useful parameters commonly employed are the relative viscosity ( $\eta/\eta^\circ$ ) and the relative viscosity change ( $[\eta - \eta^\circ]/\eta^\circ \equiv \Delta\eta/\eta^\circ$ ) which have been differently correlated with electrolyte molarity ( $c$ ) or molality ( $m$ ) by various workers.<sup>26,51,52</sup> A cubic polynomial (isotherm) in  $m$  can readily be transformed into the Jones–Dole<sup>52–54</sup> type relation as below

$$\frac{\eta - \eta^\circ}{\eta^\circ} \equiv \frac{\Delta\eta}{\eta^\circ} \equiv B \cdot m + C \cdot m^2 + D \cdot m^3 \quad (6)$$

where  $\eta^\circ$  and  $\eta$  are, respectively, the viscosities of the solvent (without LiCl) and solution at any given temperature. Various terms on the right-hand side of eq 6 contribute toward  $\Delta\eta/\eta^\circ$ , each becoming relatively more significant at higher LiCl concentrations ( $m \geq 4.5$ ). Coefficients  $B$ ,  $C$ , and  $D$  are listed



**Figure 8.** (a–d) Temperature variation of coefficients  $k_i$  of the isotherm  $\kappa(T) = k_1 \cdot m + k_2 \cdot m^2 + k_3 \cdot m^3$  for aqueous ethanol of different water mole fractions,  $x_1$ . (a)  $x_1 = 0.9$ , (b)  $x_1 = 0.7$ , (c)  $x_1 = 0.4$ , and (d)  $x_1 = 0.1$ .



**Figure 9.** (a–d) Coefficients  $k_i$  of Figure 8 plotted against water mole fraction,  $x_1$ , at different temperatures: (a) 5 °C, (b) 20 °C, (c) 35 °C, and (d) 50 °C.

in Table 6 which apparently do not exhibit any regular trend and correlation for different solvent mixtures; however, for a given mixture, temperature variation of the coefficients is quite consistent.  $B$  takes into account the solute–solvent interactions (ion–solvent for the electrolyte solutions) making it rather more important over the entire concentration range of the solute, while  $C$  signifies the solute–solute interactions.<sup>24,54–57</sup> It has been suggested regarding  $D$  that it should reflect

variation in the solvent (1)–solvent (2) interactions, more importantly as a consequence of selective solvation of solute by one of the solvent components.<sup>58</sup> For all the mixtures, the solution viscosity throughout increased with LiCl concentration, a typical behavior exhibited by structure-making electrolytes also recognized from the positive  $B$ -values.<sup>53</sup>

In the selected temperature range of study, a significant viscosity decrease has been observed on raising the temperature,

particularly for the solutions having higher LiCl concentrations. Viscosity is generally correlated with temperature by the Arrhenius-type relationship

$$\ln \eta = \ln \eta_{\infty} + \frac{E_a}{RT} \quad (7)$$

where  $\eta_{\infty}$ ,  $E_a$ , and  $R$  are, respectively, the “infinite temperature” viscosity, flow activation energy, and the gas constant. In accordance with eq 7, our  $\ln \eta$  versus  $1/T$  plots for the system are fairly straight (plots for solutions in some selected mixtures are given in Figure 5a–d), while all the determined activation energies have been listed in Table 7.  $E_a$  for the solvent mixtures are in agreement with the reported values,<sup>59</sup> but the estimated uncertainty of our  $E_a$  values could be  $\pm 5\%$ . For a given solvent (mixture),  $E_a$  always increased with LiCl concentration; however, the increase appears to be more prominent for the ethanol-rich mixtures. Plots of  $E_a$  against water mole fraction ( $x_1$ ) at various LiCl concentrations are shown in Figure 6 which tend to pass through maxima at  $x_1 \approx 0.6$ , the composition at which the  $V^E$  isotherms exhibit their minima. Belda and co-workers<sup>59,60</sup> have, however, reported the  $E_a$  maximum at a slightly higher water mole fraction of  $\sim 0.7$ .

The entire electrical conductivity data have been collected in Table 8, and the data for some selected solvent mixtures are plotted as isotherms against the LiCl aquamolality in Figure 7a–d. Each  $\kappa$  vs  $m$  plot passes through a maximum, and such results have been previously reported for other systems as well.<sup>61–63</sup> The initial sharp rise of conductivity with LiCl concentration is obviously dominated by an increased number of ions. However, on further increasing the concentration, besides higher viscosities, phenomena involving ionic interactions<sup>33</sup> cause a decrease of conductivities after passing through the maxima. As a simplified model, it may be considered that conductivity results from two sets of oppositely acting terms, namely,  $\kappa_{\text{up}}$  and  $\kappa_{\text{down}}$ . While there is a direct relation between  $\kappa_{\text{up}}$  and number of solvates,  $\kappa_{\text{down}}$  should include contributions arising due to ion–ion interactions, sharing of solvation spheres by the same solvent molecules, etc. Higher conductivities have been measured at higher temperatures in all cases mainly due to the decrease of the viscosity values. The conductivity data fit very well to the following polynomial in LiCl aquamolality,  $m$  ( $k_0$  has to be zero to justify a zero value of  $\kappa$  at  $m = 0$ )

$$\kappa(T) = k_0 + k_1 \cdot m + k_2 \cdot m^2 + k_3 \cdot m^3 \quad (8)$$

where the coefficients  $k_i$  (collected in Table 9) vary with both temperature and solvent composition. Some selected plots to demonstrate typical dependence of  $k_i$  on temperature and solvent composition are presented in Figure 8a–d and Figure 9a–d, respectively. The term involving  $k_3$  can generally be ignored due to its negligible contribution (except in water). Consequently eq 8 simplifies as

$$\kappa(T) = k_1 \cdot m + k_2 \cdot m^2 \quad (9)$$

The two terms on the right-hand side may well be regarded as  $\kappa_{\text{up}}$  and  $\kappa_{\text{down}}$ , respectively. A sharper increase of  $k_1$  beyond a water mole fraction of 0.8 (Figure 9) suggests higher mobility of the aquo-solvates,<sup>64</sup> which is further supported by shifting of the conductivity maximum from  $\sim 4.5m$  in the ethanol-rich solvents ( $x_1 < 0.5$ ) to  $\sim 6m$  in the water-rich mixtures ( $x_1 > 0.5$ ).

Conductivity and viscosity, both being transport properties, are also related to each other in different ways.<sup>65</sup> Accordingly the molar conductivity,  $\Lambda_m$ , may also be considered to follow the Arrhenius relationship (eq 10). The corresponding conduc-

tivity activation energy,  $E_c$ , can readily be determined from the temperature dependent measurements.

$$\Lambda_m(T) = \Lambda^{\infty} e^{-E_c/RT} \quad (10)$$

$\Lambda^{\infty}$  is the molar conductivity at the so-called “infinite temperature”, and the other symbols have the usual meanings.  $E_c$  determined from the slopes of  $\ln \Lambda_m$  vs  $1/T$  plots are also given in Table 7. The  $E_c$  values come out smaller than the corresponding viscosity  $E_a$  values. A possible explanation is that the ion transport under the influence of the applied electrical field involves movement of the individual solvates in the solution, whereas in the case of viscous flow under the influence of mechanical force, the whole layer of liquid has to move experiencing a higher barrier. Like  $E_a$ , also the  $E_c$  values tend to pass through a maximum for the system but at a water mole fraction of  $\sim 0.8$ .

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